

### City of Hastings Wellhead Protection Plan Amendment

Part I:

Delineation of the Wellhead Protection Area (WHPA), Drinking Water Supply Management Area (DWSMA), and Assessments of Well and DWSMA Vulnerability

Prepared for City of Hastings

November 2019

### City of Hastings Wellhead Protection Plan Amendment

### November 2019

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#### Certifications

I hereby certify that this plan, document, or report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Geologist under the laws of the state of Minnesota.						
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#### General Information

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UNIQUE WELL NUMBER(S) <u>206333, 207993, 207639, 207643, 509053, 686266</u>

SIZE OF POPULATION SERVED <u>22,713 (2018 estimate)</u>

COUNTY <u>Dakota</u>

### **Executive Summary**

**Protection Areas** - The recharge area for the wells is known as the wellhead protection area, or WHPA, and represents the area that contributes water to the City's wells within a 10-year time period. For Hastings, the WHPA includes a groundwater contribution area and a surface water contribution area because the Vermillion River is known to contribute water to the aquifer near Hastings. The area that contributes water within a one-year time period is known as the emergency response area, or ERA. Practical reasons require the designation of a management area that fully envelops the WHPA, called the drinking water supply management area, or DWSMA. This report describes how a new WHPA and DWSMA, shown on Figure 8, were delineated for the City of Hastings.

**Geology and Groundwater Flow** – The city of Hastings has 6 primary water supply wells. Wells 3, 4, 5, 6, 7, and 8 draw water from the Jordan Sandstone aquifer between 188 and 400 feet below ground surface (ft bgs). Regionally, groundwater flow is to the northeast toward the Mississippi River. Well construction information is summarized in Table 2.

**Well Vulnerability** - The vulnerability of each individual well has been assessed based on 1) well construction details, especially conformance with standards required by the State well code, 2) the geologic sensitivity of the aquifer, and 3) past monitoring results. Wells 3, 4, 5, 6, 7, and 8 are considered vulnerable to contamination based on water quality data (Table 5).

**DWSMA vulnerability** -The vulnerability of the City's aquifer throughout the DWSMA is based on a published pollution sensitivity map for the Prairie du Chien-Jordan aquifer, the geologic sensitivity ratings of wells in and near Hastings, and tritium data from Wells 4, 6, and 7. Based on this information, high vulnerability has been assigned to the entire DWSMA. High vulnerability suggests that water, and any contaminants, may travel from the land surface to the City's aquifer within a time span of months to a few years.

**Water Quality Concerns** - At present, none of the contaminants for which the Safe Drinking Water Act has established health-based standards are found above maximum allowable levels in the City's water supply. E. coli bacteria were detected on September 22, 2018 and temporary ongoing disinfection has been implemented, with a permanent gas-chlorine disinfection system scheduled to be fully online by June of 2020. The highest nitrate concentration detected in 2018 was 9.4 ppm, near the MCL of 10 ppm. Nitrate levels are discussed further in Section 6.0 of this report.

**Recommendations** - Recommendations have been generated to improve future delineations and vulnerability assessments and should be considered for inclusion as management strategies in the City's wellhead protection plan. These recommended activities include water quality monitoring, details of which can be found in Section 7.0 of this report.

#### 1.0 Introduction

In compliance with the Minnesota Wellhead Protection Rules (MN Rules 4720.5100 through 4720.5590), a Wellhead Protection Area (WHPA) and a Drinking Water Supply Management Area (DWSMA) were delineated for the City of Hastings in 2009 (Barr, 2009). Minnesota Rule 4720.5570 states that wellhead protection plans must be reviewed and amended at least every ten years.

As required by Minnesota Rule 4720.5570, a new WHPA and a new DWSMA have been delineated for the City of Hastings. This report summarizes work completed to update the delineation of the Hastings WHPA and DWSMA in compliance with the Minnesota Wellhead Protection Rules and to meet the current MDH requirements. Data elements used in preparation of the report are presented in Table 1.

The City of Hastings currently has 6 primary municipal water supply wells. All 6 wells are completed in the Jordan Sandstone aquifer. Well locations are shown on Figure 1. Table 2 summarizes construction, use, and vulnerability information for the Hastings water supply wells. Appendix A contains well logs for the City's wells.

#### 2.0 Criteria for Wellhead Protection Area Delineation

The following criteria were used to ensure accurate delineation of the WHPA.

#### 2.1 Time of Travel

A minimum 10-year groundwater time of travel criterion must be used to delineate a WHPA (MN Rule 4720.5510) so there is sufficient reaction time to remediate potential health impacts in the event of contamination of the aquifer. A groundwater time of travel of ten years was considered in this study. As required by the Wellhead Protection Rules, the one-year groundwater time of travel zone was also determined for each well addressed in this study.

#### 2.2 Aquifer Transmissivity

For this study, the transmissivity of the Jordan Sandstone aquifer was estimated using a pumping test conducted at Well 5 in 2003. Wells 3 and 4 were used as observation wells. Analysis of the data for this test estimated a representative Jordan transmissivity of 5,444 ft²/day (505.8 m²/day). The average aquifer thickness at Wells 3, 4, and 5 of 95.7 feet (29.2 m) was used to compute a representative hydraulic conductivity of 56.9 ft/day (17.3 m/day). A summary of the aquifer test is included in Appendix B. See Section 2.5 below for details regarding how this hydraulic conductivity value was incorporated into the groundwater model.

#### 2.3 Daily Volume of Water Pumped

Pumping data for the City of Hastings for the period 2014 through 2018 are in Table 3. The largest annual withdrawal for 2014-2018 was 899,740,000 gallons in 2014. The City's Local Water Supply Plan projects a 2024 average daily demand of 2.63 million gallons per day. Projected 2024 pumping rates for each well were calculated by multiplying the total 2024 projected demand by the 2014-2018 average percentage of total withdrawal for each well. The pumping rate used in the model for each Hastings well for the WHPA delineation was either this 2024 projection or the historical maximum for the period 2014-2018, whichever was greater. The pumping rates used in the model for delineation of the WHPA are in Table 3. Unaccounted water (the difference between the total volume pumped annually by the City's wells and the total amount billed to users) is approximately 10-15%.

#### 2.4 Conceptual Hydrogeologic Model

The regional hydrogeologic conceptual model is presented in Metropolitan Council (2009). Additional geological information is included below, along with discussion of groundwater flow boundaries and flow directions specific to the Hastings area.

#### 2.4.1 Regional Bedrock Geology

A bedrock map derived from the Twin Cities ten-county metropolitan area geologic map (Mossler, 2013) is shown on Figure 1. Locations of two geologic cross sections through the study area are also shown on

Figure 1. Geologic cross section A-A' (Figure 2) is a north to south cross section that intersects northwest to southeast cross section B-B' (Figure 3) at Well 5.

The hydrostratigraphic units of importance for this study are described in more detail below.

#### Jordan Sandstone

The Cambrian-aged Jordan Sandstone consists of two interlayered facies: a fine- to coarse-grained, friable, quartz sandstone and a very fine-grained, feldspathic sandstone with lenses of siltstone and shale (Mossler, 2013). Where it is not eroded the Jordan Sandstone is typically 85 to 100 feet thick. As shown on Figure 1, the Jordan Sandstone is the uppermost bedrock along the margins of the bedrock valleys in and near Hastings and has been completely eroded away within the bedrock valleys.

#### Prairie du Chien Group

The Ordovician-aged Prairie du Chien Group is divided into two formations: the upper Shakopee Formation and the lower Oneota Dolomite. The Shakopee Formation is a heterolithic unit composed of dolostone, sandy dolostone, and sandstone, while the Oneota Dolomite is medium- to thick-bedded dolomite (Mossler, 2013). The Prairie du Chien Group is the uppermost bedrock across much of Hastings. It ranges in thickness from 136 to 268 feet where encountered at Hastings' wells. The Prairie du Chien Group is classified as being highly fractured over much of the Twin Cities metropolitan area, especially under shallow bedrock conditions (overlying bedrock thickness < 200 feet, after Runkel et al. (2003)). Groundwater in the Prairie du Chien Group flows through joints, fractures, and bedding planes (Palen, 1990). No Hastings wells are open to the Prairie du Chien Group, but it is hydraulically connected to the underlying Jordan Sandstone.

#### 2.4.2 Flow Boundaries

The Mississippi River to the north of Hastings is a regional groundwater flow boundary. Figure 1 also shows several faults in the Hastings area. These faults were not explicitly represented in the groundwater flow model (Section 2.5) but were accounted for in the fracture flow delineation (Section 3.2).

#### 2.5 Model Description

To accurately delineate the WHPAs, it is necessary to assess how nearby wells, rivers, lakes, and variations in geologic conditions affect groundwater flow directions and velocities in the aquifer. A groundwater model constructed using the finite difference code MODFLOW-96 (Harbaugh and McDonald, 1996) was used for this study to simulate groundwater flow in the hydrostratigraphic units from the Quaternary aquifer down to the Mt. Simon Sandstone. MODFLOW-96 is public domain software that is available at no cost from the United States Geological Survey. The pre- and post-processor Groundwater Vistas (version 7) (Environmental Simulations, Inc., 2017) was used to create the model data files and evaluate the model results.

#### 2.5.1 Base Model

Consistent with the Scoping Letter (MDH, 2018), the base model used in this study is the same model used for the 2009 Hastings WHPP. The model is based on Metro Model 2 (Metropolitan Council, 2009),

which was developed by Barr Engineering for the Metropolitan Council to assist in evaluating groundwater use and water sustainability issues, regional water planning issues, and groundwater appropriations.

The model is divided into 9 layers to represent the major hydrostatigraphic units in the Twin Cities Metropolitan Area. In Hastings, the model layers represent the following (ordered from youngest to oldest; i.e., shallowest to deepest):

- Layer 1: Quaternary glacial drift
- Layer 2: St. Peter Sandstone or Quaternary glacial drift (where present)
- Layer 3: Prairie du Chien Group or Quaternary glacial drift (where present)
- Layer 4: Jordan Sandstone or Quaternary glacial drift (where present)
- Layer 5: St. Lawrence Formation or Quaternary glacial drift (where present)
- Layer 6: Tunnel City Group
- Layer 7: Wonewoc Sandstone
- Layer 8: Eau Claire Formation
- Layer 9: Mt. Simon Sandstone

Major rivers near Hastings (i.e., the Mississippi, Vermillion, and St. Croix Rivers) are simulated using the River Package within MODFLOW. Baseflow measurements for rivers and streams in the area were used during calibration of Metro Model 2.

Recharge for the groundwater flow model was determined using the SWB recharge model (Westenbroek et. al., 2010) of the Twin Cities Metropolitan Area (Metropolitan Council, 2009). Monthly precipitation data for Hastings from the last 5 years is summarized in Table 4.

Modifications made to the base model for the new Hastings WHPA delineations are discussed in the following section.

#### 2.5.2 Model Modifications and Updates

The following modifications and updates were made to the base model:

- The edges of the Prairie du Chien Group and Jordan Sandstone within the refined grid area were revised to more closely follow the bedrock map (Mossler, 2013).
- The horizontal hydraulic conductivity value (Kx) for the Jordan in zone 346, which includes all of the Hastings wells, was updated to 17.3 m/day to match the aquifer test plan (Appendix B). A vertical anisotropy ratio (Kx/Kz) of 10 was assumed for zone 346. Appendix C includes a map of model hydraulic conductivity field for Layer 4 in the Hastings area (Figure C1).
- The pumping rates for the City's wells were changed to the model input rates shown in Table 3.
- Pumping rates for 23 high-capacity wells within 2 miles of Hastings were updated to use 2013-2017 averages. A list of these wells is included as Table C1 in Appendix C. Nine of these wells (unique numbers listed below) were added to the model because they were not included in the model used for the 2009 WHPP:

- o 170868, permit 1975-6358
- o 250020, permit 1976-6157
- o 250177, permit 1969-1102
- o 257402, permit 1976-6204
- o 749829, permit 1985-6224
- o 768670, permit 2015-1357
- o 771760, permit 1985-6224
- o 806056, permit 2015-1392
- o (no unique number), permit 1993-6152
- After the above modifications were made, modeled heads were compared to observed heads from Minnesota Well Index records located within the model domain. No further calibration was deemed necessary. A plot of modeled versus measured heads is included as Figure C2 in Appendix C. Full discussion of the Metro Model 2 calibration is presented in Metropolitan Council (2009).

MODFLOW files for the updated model are included in Appendix I.

#### 2.6 Groundwater Flow Field

The groundwater flow field used for delineation of the WHPA was determined by the groundwater flow model; modeled contours for the Jordan Sandstone/Quaternary glacial drift (Layer 4) are shown on Figure 4.

In general, Figure 4 shows the Jordan flow direction in Hastings to be northeasterly toward the Mississippi River. The modeled northeasterly flow direction is consistent with a published contour map for the Prairie du Chien – Jordan aquifer from the Dakota County Geologic Atlas (Palen, 1990). Based on this comparison and the acceptable calibration of the groundwater model, the groundwater flow field was determined to be of acceptable accuracy for the WHPA delineation.

#### 3.0 Delineation of the Wellhead Protection Area

Delineation of the WHPA for the Hastings wells involved the evaluation of porous media flow, fracture flow, and surface water contribution (conjunctive delineation) as detailed below.

#### 3.1 Porous Media Flow Evaluation

The groundwater flow model discussed above in Section 2 was used to simulate the groundwater flow field in the vicinity of Hastings. The porous media capture zone for the Hastings well field was delineated using the software program MODPATH (Version 3; Pollock, 1994) with the modeled groundwater flow field. A minimum of 180 particles were tracked from each well. The particles were released from up to 6 vertical points in each layer along the open interval of each well. These particles were tracked backwards in time for both one and ten years. In plan view, the areas encompassed by the particle traces were then outlined as the 1-year and 10-year porous media time of travel zones for the well field.

Porosity values used for the porous media flow evaluation were as follows (Norvitch et al., 1974, Schwartz and Zhang, 2003):

- Quaternary Glacial Drift = 0.25
- St. Peter Sandstone = 0.283
- Prairie du Chien Group = 0.056
- Jordan Sandstone = 0.2

#### 3.1.1 Sensitivity Analysis

A sensitivity analysis was performed to test the sensitivity of the model results to varying hydraulic conductivity in the Jordan Sandstone aquifer. Lower and upper bounds of 20.1 ft/day (6.1 m/day) and 191 ft/day (58.1 m/day), respectively, were tested for horizontal Jordan hydraulic conductivity. These values were derived from the pumping test transmissivity ranges (Appendix B). A vertical anisotropy ratio of 10 was assumed for both sensitivity runs. A plot of the sensitivity analysis results is included in Appendix C (Figure C3).

Multiple particle tracking simulations were conducted to account for uncertainty in the groundwater flow model. In addition to the base model run, particle tracking simulations were also conducted for both of the sensitivity runs. Particle traces from all simulations were used to delineate the 1-year and 10-year porous media capture zones for each well. These capture zones are shown on Figure 5.

#### 3.2 Fracture Flow Evaluation

All of Hastings' wells are open to the Jordan Sandstone, which is likely hydraulically connected to the overlying Prairie du Chien Group. To address fracture flow in the Prairie du Chien Group, MDH (2011a) guidelines for delineating WHPAs in fractured and solution-weathered bedrock were followed using Delineation Technique Number 4 (wells open only to a porous media aquifer that is hydraulically connected to a fractured or solution-weathered aquifer). In addition, the fracture flow capture zones were

also extended along two fault orientations. A summary of the calculations used in the delineation of fracture flow capture zones is presented in Appendix D.

#### 3.2.1 Fixed Radius Capture Zones and Upgradient Extensions

Although the Hastings wells are open to only the Jordan Sandstone, a porous media aquifer, the porous media modeling suggests that the Jordan Sandstone is hydraulically connected to the fractured and solution-weathered Prairie du Chien Group. The water budget software ZONEBUDGET (Harbaugh, 1990) was used to compute the contributions from model layer 3 (Prairie du Chien Group) to the baseline 10-year porous media capture zones in layer 4 (Jordan Sandstone) for each well. Flow from model layer 3 to model layer 4 within the capture zones ranged from 20% at Well 5 to 76% at Well 3 (Table D1 in Appendix D). The MDH guidelines cite a threshold of 10% for determining whether or not recharge from the fractured or solution-weathered aquifer is a significant source of recharge to the porous media aquifer; because the calculated percentages for all Hastings wells were above this threshold, it was necessary to delineate fracture flow capture zones for all wells.

Note that the Prairie du Chien Group is not present at Well 3 (Figure 1). Because the Prairie du Chien is present upgradient of Well 3 and the modeled particle traces from Well 3 travel upgradient into the Prairie du Chien, fracture flow capture zones were delineated for Well 3. The Prairie du Chien thickness at Well 5 was assumed for the purposes of the Well 3 fracture flow calculations.

The ratio of the well discharge to the discharge vector was calculated for each well using the contribution from model layer 3 calculated by ZONEBUDGET as the pumping rate. This ratio was less than 3,000 for all wells, so upgradient extensions were required for the 1-year and 10-year fracture flow capture zones. Hydraulic gradients and upgradient directions (i.e., bearings) were estimated from the baseline model layer 3 flow field.

For the 1-year time of travel, 6-month fixed-radius capture zones and 6-month upgradient extensions were delineated for each individual well using the GIS-based MDH Fracture Flow Tool. For the 10-year time of travel, 5-year fixed-radius capture zones and 5-year upgradient extensions were delineated for each individual well using the MDH Fracture Flow Tool. Table D2 in Appendix D is a summary of the inputs to the Fracture Flow Tool.

To evaluate the potential for overlapping capture zones, 10-year fixed-radius capture zones were calculated for 10 nearby wells as documented in Table D3 in Appendix D. Four of these capture zones (for wells 255924, 251398, 771760, and 207640) overlapped with the preliminary 5-year fixed radius capture zones for three of the Hastings wells (4, 7, and 8). The overlapping areas were calculated using geometric functions within ArcGIS, which allows for a more accurate redistribution of the shared volumes than the method described in the MDH fracture flow guidelines. The areas of the preliminary 5-year fixed radius capture zones for Wells 4, 7, and 8 were adjusted to include the overlapping areas, and the effective pumping rate necessary to generate the enlarged areas was calculated. These effective pumping rates were then used as input to the MDH Fracture Flow Tool to generate the final 10-year capture zones (5-year fixed radius and 5-year upgradient extension). The MDH 2-Well Fracture Flow Tool was used to

account for the slight overlap between the adjusted 5-year fixed radius capture zones for Wells 3 and 7 and for Wells 6 and 8.

The final 5-year fixed-radius fracture flow capture zones and upgradient extensions were truncated at the extents of the Prairie du Chien Group. The truncated capture zones are shown on Figure 6.

#### 3.2.2 Fault Extensions

As discussed at the Predelineation Meeting (MDH, 2019), the 5-year fixed-radius capture zones were extended along two perceived fault orientations (Mossler, 2013): N 52 E (52° / 232°) and N 33 W (123° / 303°). Per the MDH fracture flow guidelines, the capture zones were extended 1 mile from each well along the fault orientations. Because the faults extend through the Jordan Sandstone (Figures 2 and 3), the fault extensions were truncated at the extents of the Jordan Sandstone instead of the extents of the Prairie du Chien Group, as was done for the fixed-radius capture zones and upgradient extensions. The fault extensions were also truncated at the Mississippi River as it constitutes a major hydraulic boundary. The truncated fault extensions are shown on Figure 6.

#### 3.3 Conjunctive Delineation

It is recognized that the Vermillion River is a losing stream west of Hastings. Water samples from the city wells indicate water of relatively young age based on nitrate levels (Dakota County, 2003), and oxygen and hydrogen isotope data indicate a surface water signature in the water from Wells 4 and 6 (Appendix E). Because the Vermillion River is potentially a source of water for the city wells, a surface-water contribution area is required. Because the new groundwater capture area is not significantly different than that from the 2009 delineation, a new surface water contribution area was not delineated and the 2009 surface water contribution area was reused with minor adjustments in Hastings where it coincides with the groundwater capture zone. The surface water contribution area is shown on Figure 7.

#### 3.4 WHPA Delineations

The composite 10-year porous media capture zones, 5-year fixed radius fracture flow capture zones, and 5-year upgradient extensions define Area A of the WHPA. The boundaries of Area A were slightly simplified from the merged capture zones to eliminate "holes" between individual capture zones. The surface water contribution area defines Area B of the WHPA. Much of the groundwater within Area B does not flow to Hastings. However, surface-water runoff within Area B has the potential to reach the Hastings wells via seepage from the Vermillion River. The Emergency Response Area (ERA) is delineated for each well by the composite 1-year porous media capture zones and composite 1-year fracture flow capture zones. The WHPA and ERAs are shown on Figure 8.

### 4.0 Delineation of the Drinking Water Supply Management Area

The Hastings DWSMA encompasses WHPA Areas A and B with boundaries that correspond to geographically identifiable features (e.g., roads, parcel boundaries, quarter-quarter section lines). Like the WHPA, the DWSMA is broken down into two areas; Area A comprising the groundwater capture zones, and Area B comprising the surface water contribution area. Property parcel boundaries were used to define Area A while quarter-quarter section boundaries were used to define Area B. The Hastings DWSMA is shown on Figure 8. To satisfy Minnesota Rule 4720.5500, Subpart 2, 1:24,000 scale maps of the DWSMAs are included in Appendix F.

### 5.0 Well Vulnerability Assessment

MDH evaluated the vulnerability of the Hastings municipal wells to contamination from contaminants released at the surface. The evaluation parameters include geology, well construction, pumping rate, and water quality. All Hastings wells are classified as "vulnerable." Copies of the MDH well vulnerability scoring sheets for the Hastings wells are included in Appendix G.

# 6.0 Drinking Water Supply Management Area Vulnerability Assessment

The vulnerability of the Jordan Sandstone within the DWSMA associated with the Hastings wells was evaluated in a manner consistent with MDH guidance for assessing aquifer vulnerability (MDH, 1997) using a published pollution sensitivity map (Hobbs, 1990), geologic sensitivities based on L scores computed from boring log data, and water quality data from the Hastings wells.

The first step in the assessment is to determine the geologic sensitivity rating of the aquifer. The Minnesota Department of Natural Resources (MnDNR) defines geologic sensitivity based on the travel time of water moving vertically from the surface to the aquifer of interest as follows (see MnDNR, 1991):

- Sensitivity = Very High: vertical travel time is hours to weeks
- Sensitivity = High: vertical travel time is weeks to years
- Sensitivity = Moderate: vertical travel time is years to decades
- Sensitivity = Low: vertical travel time is several decades to a century
- Sensitivity = Very Low: vertical travel time is more than a century.

The pollution sensitivity map for the Prairie du Chien – Jordan aquifer from the Dakota County Geologic Atlas (Hobbs, 1990) was used as a starting point for developing the Jordan Sandstone geologic sensitivity map. This map includes "High-Moderate" and "Low-Moderate" ratings which are not recognized by MDH. Based on the definitions of "High-Moderate" as a travel time of "years to a decade" and "Low-Moderate" as a travel time of "several decades", these areas were remapped to the "Moderate" and "Low" ratings, respectively, on the MnDNR definitions above. The modified geologic sensitivity map is shown on Figure H1 in Appendix H.

"L scores" based on the thickness of low permeability units at Minnesota Well Index well locations in the vicinity of the DWSMA were computed using the MDH L score tool [See MnDNR (1991) for a discussion of how to determine L scores]. The calculated L scores are shown on Figure H1 in Appendix H.

Tritium samples were collected at Well 4 in 2004 and at Wells 6 and 7 in 2016. Tritium (<sup>3</sup>H), a radioactive isotope of hydrogen, has been used extensively to date groundwater. Tritium activities peaked during atmospheric hydrogen bomb testing of the 1950s and 1960s, and values of <sup>3</sup>H in precipitation reached a maximum of approximately 10,000 T.U. (tritium units) in 1963 (Mazor, 2004). Natural production of <sup>3</sup>H in the upper atmosphere introduces approximately 5 T.U. to precipitation each year (Mazor, 2004). Because <sup>3</sup>H has a relatively short half-life of 12.43 years, radioactive decay since the bomb peak has reduced tritium activities to near background levels and <sup>3</sup>H is used mostly for relative age dating today. Groundwater that has little or no detectible <sup>3</sup>H is stated to be "vintage" or pre-bomb. Groundwater with detectable concentrations of <sup>3</sup>H is stated to be "young" or post-bomb. The presence of tritium at concentrations above 1 tritium unit indicates the presence of a significant fraction of post-1953 (i.e., recently infiltrated) water in the groundwater sample. As shown on Table 5, tritium was detected in the samples collected from Wells 4, 6, and 7. Table 5 also shows other water quality results from sampling of the City's wells.

The presence of tritium in groundwater samples from a well suggests that the water traveled vertically from the ground surface to the aquifer in less than about 50 years. Based on this information along with the geologic sensitivity ratings and L scores, High vulnerability was assigned to the entire Area A of the DWSMA. Keeping with current MDH policy, high vulnerability was assigned to all of Area B of the DWSMA (the surface water area) as well. The final aquifer vulnerability map is shown on Figure 9.

The City is frequently monitoring nitrate levels in raw water samples at all of its municipal wells but has special focus on Wells 6 and 8. Of the wells that are not currently treated for nitrate, Wells 6 and 8 have historically had the most elevated levels. Before making a significant and permanent investment in a new treatment plant, the City will first work closely with the MDH to attempt all cost-effective solutions for maintaining delivery of water in compliance with the nitrate standard from these two wells. Should a new nitrate reduction/removal treatment plant become necessary, it is presumed that such a facility would be constructed on the site of Well 6. Water system infrastructure has been roughed in to interconnect these two well sites with a transmission main that would allow for water from Well 8 to be transported to a future treatment plant at Well 6.

### 7.0 Recommendations

As discussed in Section 6.0, it is recommended that the City work with the MDH regarding the nitrate issues at Wells 6 and 8.

It is recommended that the City consider working with the MDH to conduct tritium sampling of wells 3, 4, 5, and 8 in order to have the data available when updating the well and aquifer vulnerability assessments as part of the next wellhead protection plan amendment.

### 8.0 Supporting Data Files

The groundwater model files and GIS files are included in Appendix I. (Appendix I can be found in the "Part1" folder on the CD.)

The groundwater model can be reviewed using MODFLOW-96 (Harbaugh and McDonald, 1996). MODPATH files can be reviewed using MODPATH Version 3 (Pollock, 1994).

All coordinates in the modeling files are based on UTM NAD 83 Zone 15 N datum. Elevations are in meters above mean sea level (m MSL). Time units are days. Length units are meters.

The GIS files have been named according to the MDH conventions. Shapefiles are in UTM NAD83 Zone 15 N datum.

#### 9.0 References

- Barr Engineering Company (Barr), 2009. Re: Amendment to City of Hastings Part 1 Wellhead Protection Plan. Letter report from John Greer of Barr Engineering to Steve Robertson of MDH, dated October 26, 2009.
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### **Tables**

Table 1

#### Assessment of Data Elements Hastings WHPP Amendment

	Present and Future Implications				
Data Element	Use of the Wells	Delineation Criteria	Quality and Quantity of Well Water	Land and Groundwater Use in DWSMA	Data Source
Precipitation	М	L	М	М	Minnesota Climatology Working Group
Geology					, <u> </u>
Maps and geologic descriptions	М	Н	Н	Н	MGS, MWI
Subsurface data	М	Н	Н	Н	MGS, MDH, MWI
Borehole geophysics	М	М	М	М	MGS
Surface geophysics	L	L	L	L	Not Available
Maps and soil descriptions	L	М	М	М	MGS, NRCS
Eroding lands					
Water Resources					
Watershed units	L	L	L	L	DNR
List of public waters	L	L	L	L	DNR
Shoreland classifications					
Wetlands map					
Floodplain map  Land Use					
	1	Н	1	<u> </u>	Matura alitan Caurail Deleta Caurai
Parcel boundaries map Political boundaries map	L	L	L	L	Metropolitan Council, Dakota County MNGEO
PLS map		Ī	Ī	<u> </u>	DNR
Land use map and inventory	_	_	_	<u> </u>	DIVIN
Comprehensive land use map					
Zoning map					
Public Utility Services					
Transportation routes and corridors	L	М	L	L	MNDOT
Storm/sanitary sewers and PWS system map	L	L	L	L	City of Hastings
Oil and gas pipelines map					

#### **Definitions Used for Assessing Data Elements:**

**High (H) -** the data element has a direct impact

**Moderate (M)** - the data element has an indirect or marginal impact

**Low (L)** - the data element has little if any impact

**Shaded** - the data element was not required by MDH for preparing the WHP plan

MWI - Minnesota Well Index

DNR – Minnesota Department of Natural Resources

MNGEO - Minnesota Geospatial Information Office

MDH - Minnesota Department of Health

MNDOT – Minnesota Department of Transportation

MPCA – Minnesota Pollution Control Agency

NRCS – Natural Resources Conservation Service

SSURGO – Soil Survey Geographic Database

USGS – United States Geological Survey

Table 1

## Assessment of Data Elements (Continued) Hastings WHPP Amendment

	F		nt and F plicatio			
Data Element	Use of the Wells	Delineation Criteria	Quality and Quantity of Well Water	Land and Groundwater Use in DWSMA	Data Source	
Public drainage systems map/ list	L	L	L	L	City of Hastings	
Records of well construction, maintenance, and use	Н	Ι	L	L	City of Hastings, MWI, MDH files	
<b>Surface Water Quantity</b>						
Stream flow data	L	Г	L	L	DNR	
Ordinary high water mark data	L	L	L	L	DNR	
Permitted withdrawals	L	L	L	L	DNR	
Protected levels/flows	L	L	L	L	DNR	
Water use conflicts	L	L	L	L	DNR	
<b>Groundwater Quantity</b>						
Permitted withdrawals	Н	I	Н	Н	DNR	
Groundwater use conflicts	L	L	L	L	DNR	
Water levels	Н	Н	Н	Н	MWI, MDH	
Surface Water Quality						
Stream and lake water quality management classification						
Monitoring data summary	L	L	L	L	MPCA, MDH	
<b>Groundwater Quality</b>						
Monitoring data	Н	Н	Н	Н	MDH	
Isotopic data	Н	Н	Н	Н	MDH	
Tracer studies	L	L	L	L	Not Available	
Contamination site data	L	L	М	М	MPCA, MDH	
Property audit data from contamination sites						
MPCA and MDA spills/release reports	L	L	L	L	No relevant data available	

#### **Definitions Used for Assessing Data Elements:**

**High (H) -** the data element has a direct impact

**Moderate (M)** - the data element has an indirect or marginal impact

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Table 2
Water Supply Well Information
Hastings WHPP Amendment

Local Well ID	Unique Number	Use/ Status <sup>1</sup>	Casing Diameter (in.)	Casing Depth (ft.)	Well Depth (ft.)	Year Constructed	Aquifer	Well Vulnerability
3	206333	Р	24 x 16	208	299	1956	Jordan	Vulnerable
4	207993	Р	24 x 16	314	400	1961	Jordan	Vulnerable
5	207639	Р	30 x 24	277	356	1970	Jordan	Vulnerable
6	207643	Р	30 x 24	240	332	1972	Jordan	Vulnerable
7	509053	Р	30 x 24	205	285	1989	Jordan	Vulnerable
8	686266	Р	30 x 24	188	280	2006	Jordan	Vulnerable

<sup>&</sup>lt;sup>1</sup> P = Primary

Table 3

# Annual and Projected Pumping Rates for Hastings Wells Hastings WHPP Amendment

			Total Annual Withdrawal (gal/yr)							
Unique										
Number	Well Name	2014	2015	2016	2017	2018				
206333	3	121,075,000	116,785,000	122,351,000	116,770,000	132,275,000				
207993	4	153,550,000	175,900,000	156,850,000	173,045,000	165,010,000				
207639	5	139,850,000	127,180,000	141,430,000	112,130,000	122,065,000				
207643	6	97,880,000	108,330,000	115,525,000	103,950,000	138,920,000				
509053	7	239,430,000	207,895,000	202,720,000	225,185,000	160,510,000				
686266	8	147,955,000	112,365,000	117,055,000	106,800,000	82,450,000				
	Totals	899,740,000	848,455,000	855,931,000	837,880,000	801,230,000				

Source: City water use records

Percentage of Annual Withdrawal								
Unique Number	Well Name	2014	2015	2016	2017	2018	Average Annual % of Withdrawal	
206333	3	13.5%	13.8%	14.3%	13.9%	16.5%	14.4%	
207993	4	17.1%	20.7%	18.3%	20.7%	20.6%	19.5%	
207639	5	15.5%	15.0%	16.5%	13.4%	15.2%	15.1%	
207643	6	10.9%	12.8%	13.5%	12.4%	17.3%	13.4%	
509053	7	26.6%	24.5%	23.7%	26.9%	20.0%	24.3%	
686266	8	16.4%	13.2%	13.7%	12.7%	10.3%	13.3%	

		Projec	ted Water Use	(2024)	Maximum Total Pumping for Model Input <sup>4</sup>			
Unique Number	Well Name	Total <sup>1</sup> (gal/yr)	% of Total Projected Water Use <sup>2</sup>	Projected Well Pumpage Based on % (gal/yr) <sup>3</sup>	gal/yr	gal/day	m³/day	
206333	3		14.4%	138,611,520	138,611,520	379,758	1,438	
207993	4		19.5%	187,703,100	187,703,100	514,255	1,947	
207639	5		15.1%	145,349,580	145,349,580	398,218	1,508	
207643	6		13.4%	128,985,720	138,920,000	380,603	1,441	
509053	7		24.3%	233,906,940	239,430,000	655,973	2,483	
686266	8		13.3%	128,023,140	147,955,000	405,356	1,535	
	Totals	962,580,000	100.0%	962,580,000	997,969,200	2,734,162	10,351	

Appropriation 1,300,000,000

 $<sup>^{1}</sup>$  2024 projected average daily demand of 2.63 million gallons per day from 2016 Hastings Local Water Supply Plan

 $<sup>^{\</sup>rm 2}$  Percentages for wells based on average 2014-2018 usage per well

<sup>&</sup>lt;sup>3</sup> Projected per well pumpage based on total 2024 projected withdrawal and projected percent of total pumped by each well

<sup>&</sup>lt;sup>4</sup> For each well, the greater of the estimated pumpage based on projected 2024 withdrawal and actual annual pumpage for 2014-2018.

Hastings Precipitation Data 2014-2018 Hastings WHPP Amendment

Table 4

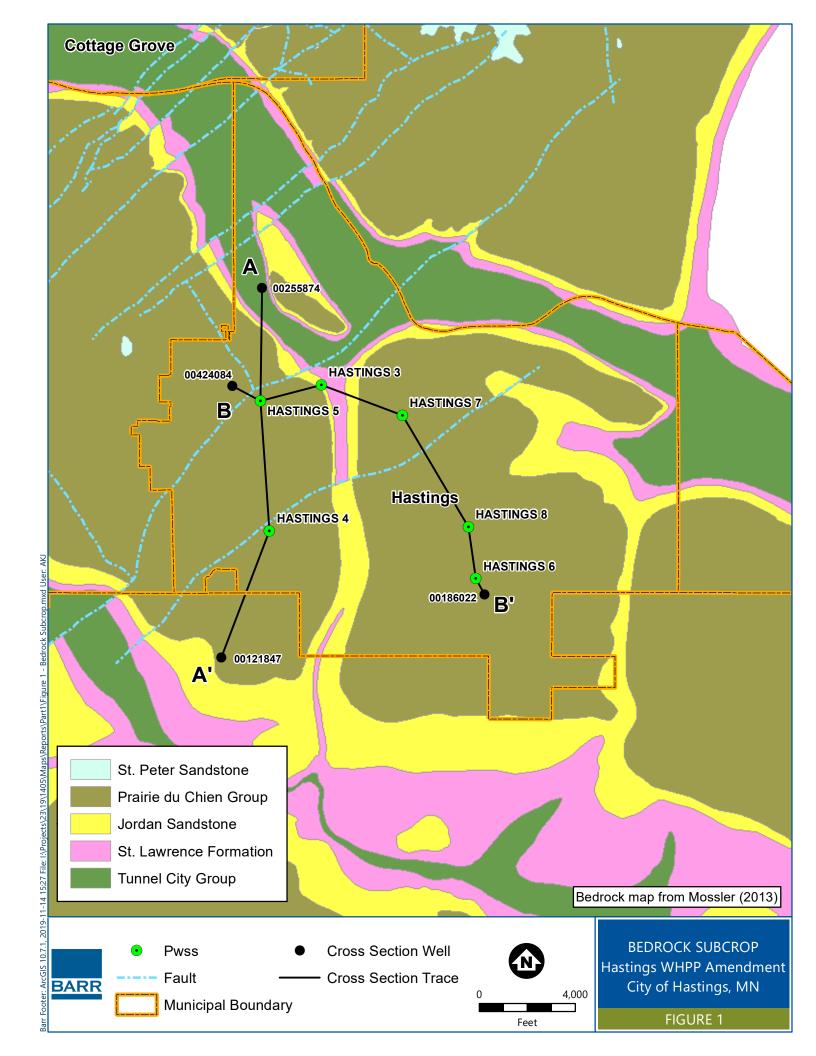
	Precipitation (inches)							
Month	2014	2015	2016	2017	2018	Average		
January	0.97	0.53	0.48	1.10	1.28	0.87		
February	1.23	0.57	0.89	0.64	0.62	0.79		
March	0.76	0.72	2.83	0.77	0.87	1.19		
April	5.79	2.24	2.62	4.45	1.66	3.35		
May	4.97	3.79	2.59	7.22	3.62	4.44		
June	10.69	5.67	4.53	3.65	6.26	6.16		
July	2.72	7.49	7.75	4.38	2.94	5.06		
August	3.39	3.84	8.47	5.09	4.62	5.08		
September	1.66	5.12	4.88	1.79	5.80	3.85		
October	1.44	2.60	2.51	4.06	3.66	2.85		
November	0.98	4.23	1.60	0.24	1.77	1.76		
December	0.63	3.19	3.03	0.63	1.32	1.76		
Total	35.23	39.99	42.18	34.02	34.42	37.17		

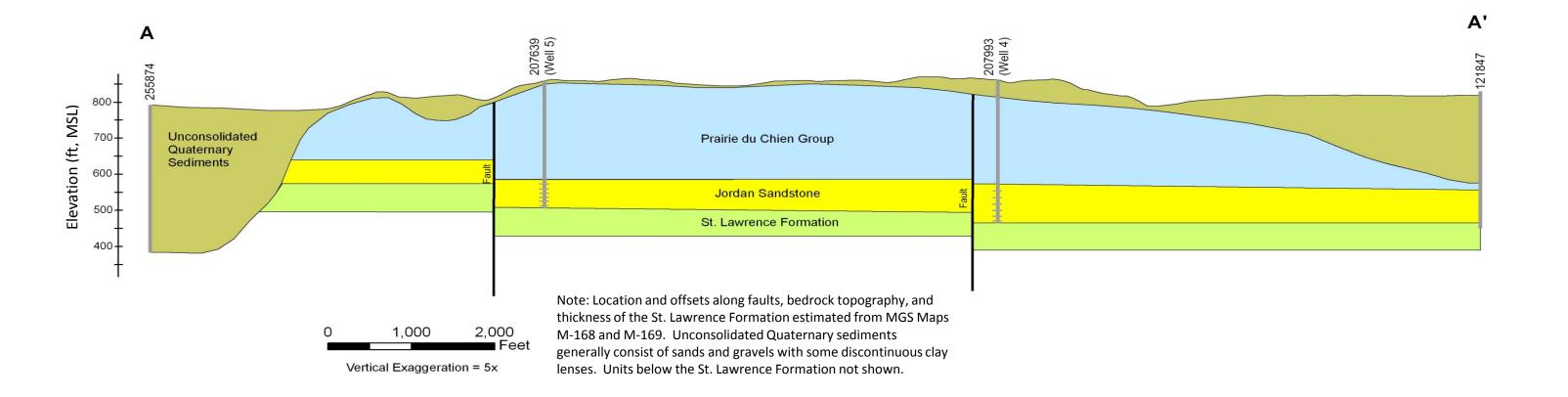
Source: Minnesota Climatology Working Group

Table 5
Hastings Water Quality Data
Hastings WHPP Amendment

Well	Tritium (TU)	Nitrate (mg/L)	Chloride (mg/L)	Bromide (mg/L)	Chloride / Bromide Ratio	Arsenic (μg/L)
3	NA	8.9 (03/12/2019)	3 (09/01/1985)	NA	NA	< 1 (01/14/1999)
4	7.6 (01/13/2004)	3.7 (03/12/2019)	14.8 (03/29/2016)	0.0322 (03/29/2016)	460 (03/29/2016)	< 1 (08/21/2012)
5	NA	8.0 (03/12/2019)	45.2 (08/21/2012)	0.0627 (08/21/2012)	721 (08/21/2012)	< 1 (08/21/2012)
6	3.7 (03/29/2016)	8.2 (01/06/2010)	22.6 (03/17/2015)	0.0346 (03/17/2015)	727 (03/17/2015)	1.47 (09/16/2004)
7	3.8 (03/29/2016) 4.36 (03/29/2016)	6.0 (03/12/2019)	39.3 (03/29/2016)	0.0444 (03/29/2016)	885 (03/29/2016)	< 1 (01/14/1999)
8	NA	7.8 (03/12/2019)	31.3 (08/21/2012)	0.0437 (08/21/2012)	716 (08/21/2012)	< 1 (08/21/2012)

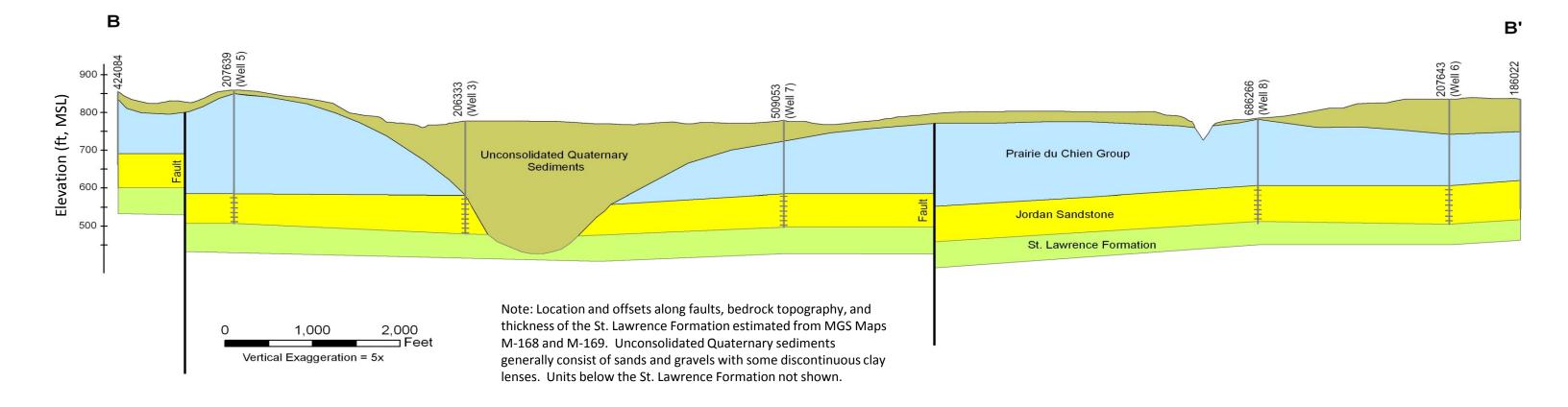
# **Figures**





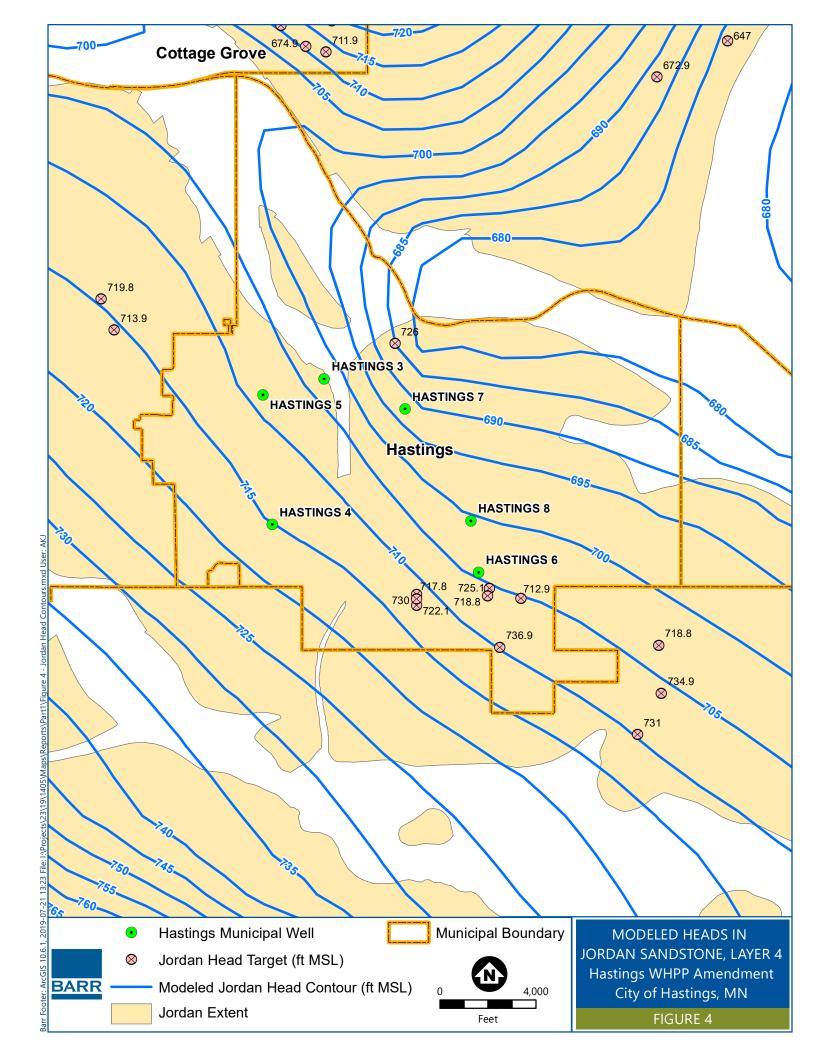


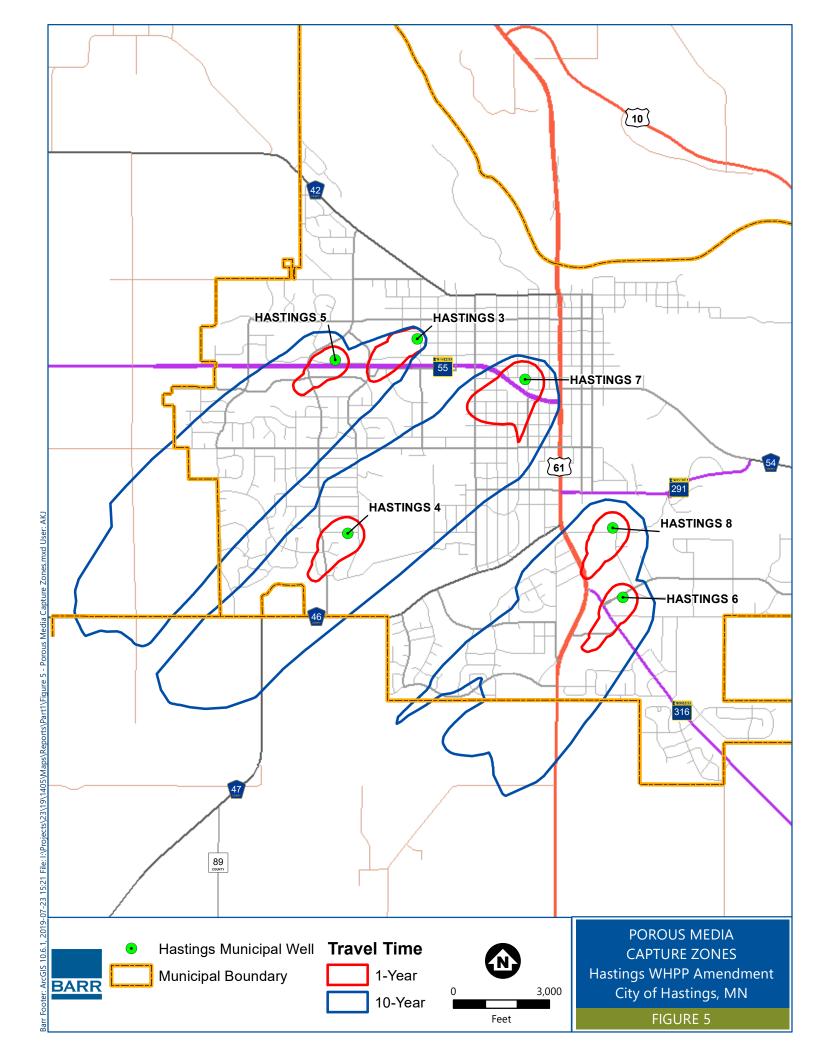
GEOLOGIC CROSS SECTION A TO A'
WHPP Amendment
City of Hastings
Dakota County, MN

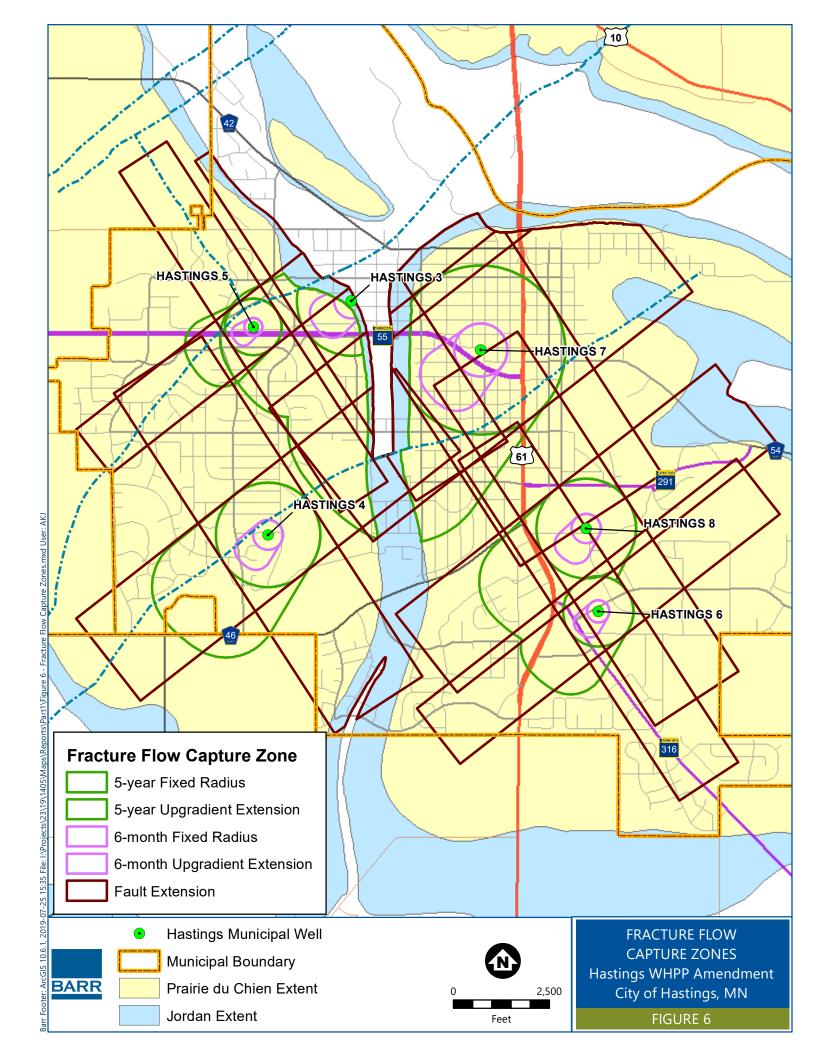


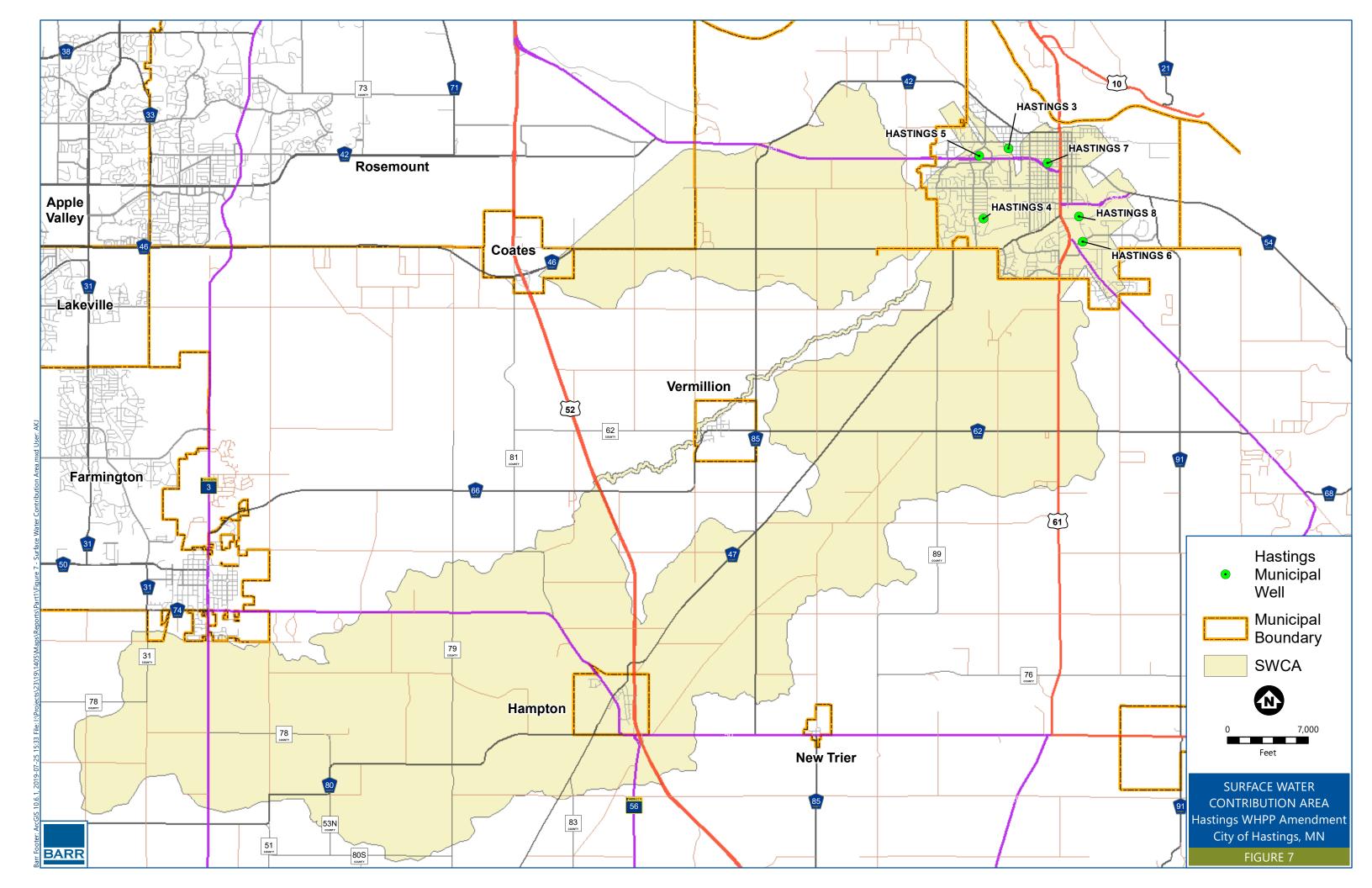


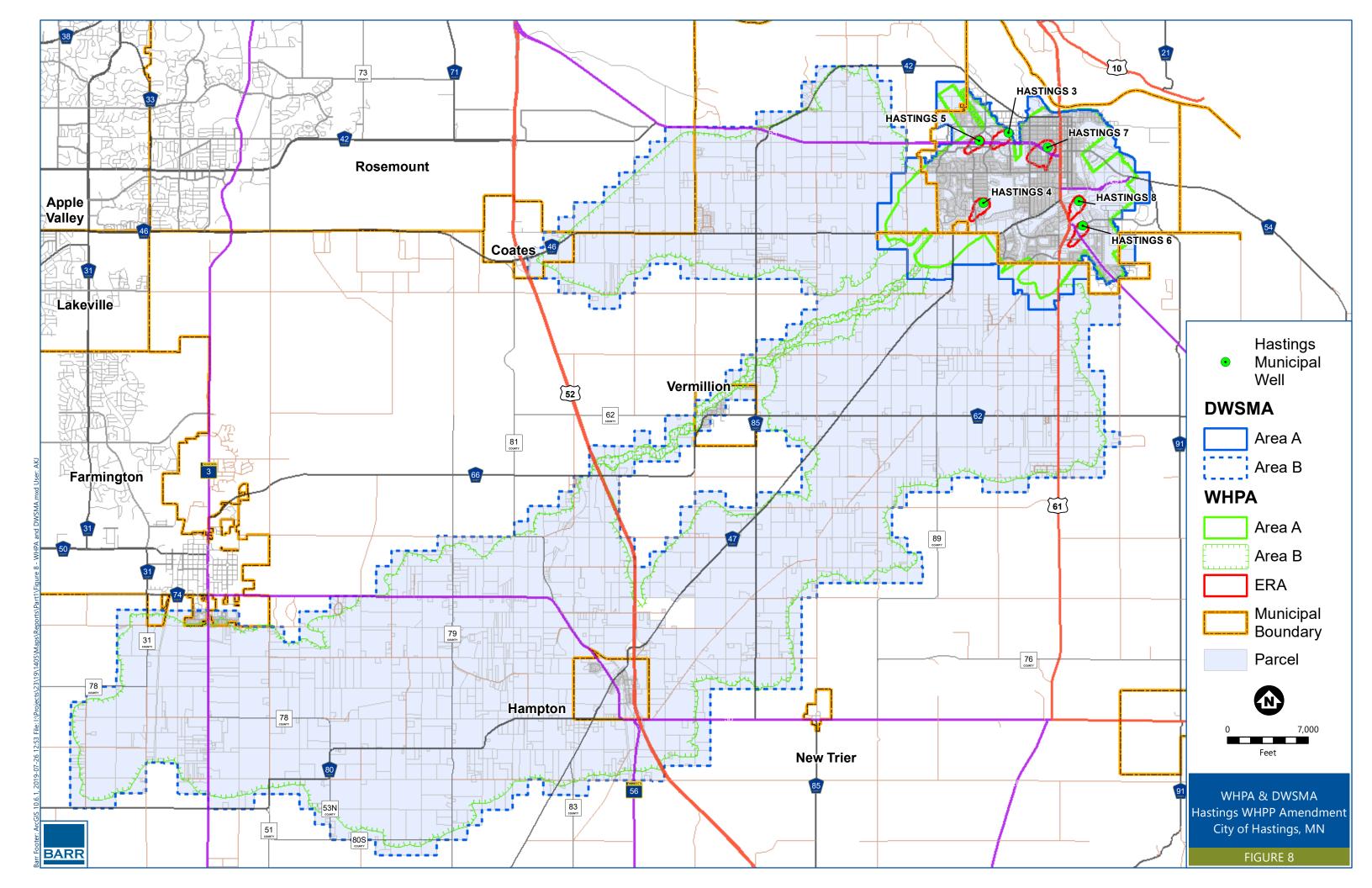
GEOLOGIC CROSS SECTION B TO B'
WHPP Amendment
City of Hastings
Dakota County, MN

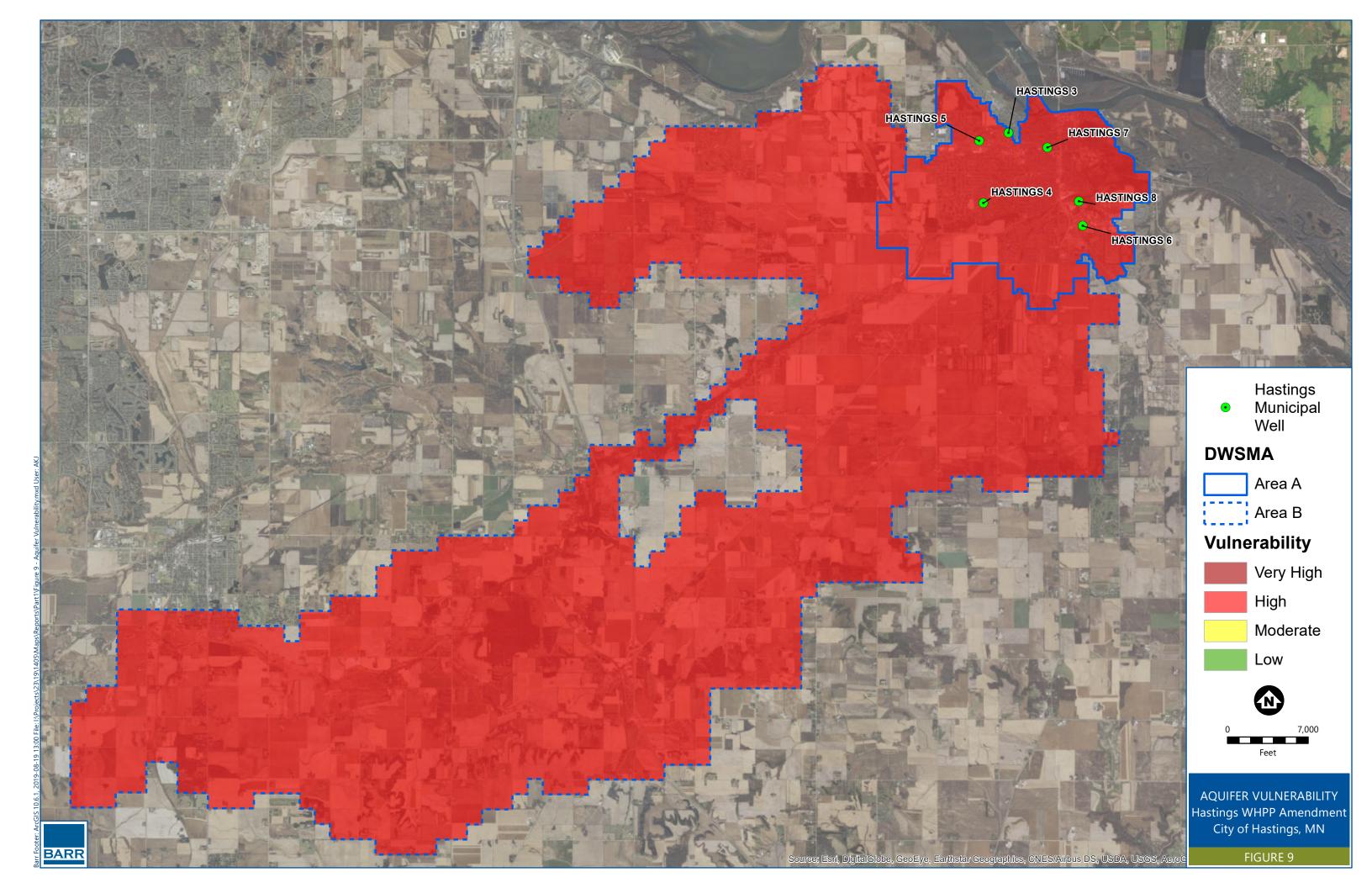












### Appendix A

**Well Construction Records** 

206333

County Dakota
Quad Hastings
Quad ID 87A

## MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

Entry Date Update Date

12/27/1989 07/11/2018

HE-01205-15

Well Name Township Range Dir Section Subsection		• •
HASTINGS 3 115 17 W 28 BCACDD		299 ft. 09/20/1956
Elevation 778 ft. Elev. Method 7.5 minute topographic map (+/		Cuote 1001 21M11MM
Address	Use co	mmunity supply(municipal) Status Active
Contact HASTINGS MN 55033	Well Hyd	ofractured? Yes No From To
Well HASTINGS MN 55033	Casing T	
Stratigraphy Information  Coologies Meterial From To (ft.) Color II	Drive Sh	75.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5
Geological Material From To (ft.) Color H CLAY 0 9	Casing D	_
SAND & GRAVEL 9 79	16 in. 7 24 in. 7	
SAND & CLAY 79 103	24 III. I	) 197 It. 108.7tt.
HARDPAN 103 107		
CLAY 107 137 BLUE		
HARDPAN 137 169	Open Ho	200
CLAY 169 176 BLUE	Screen?	Type Make
HARDPAN 176 197		
SANDROCK (JORDAN) 197 267		
SANDSTONE 267 299 GRAY	Static W	ter Level
	67 f	
	Pumping	Level (below land surface)
	115. ft	32. hrs. Pumping at 1000 g.p.m.
	Wellhea	Completion
		pter manufacturer Model
		ng Protection X 12 in. above grade
		rade (Environmental Wells and Borings ONLY)
		Information Well Grouted? X Yes No Not Specified
	Material	Amount From To
	neat cen	ont 0 0 ft. 208 ft.
	Nearest	Known Source of Contamination
	T (cur est	feet Direction Type
	Well dis	nfected upon completion? Yes No
	Pump Manufac	Not Installed Date Installed urer's name
	Model N	mber HP <u>0</u> Volt
	Length o	drop pipe ft Capacity g.p. Typ
	Abandoi	
		perty have any not in use and not sealed well(s)? Yes No
	Varianc	
	Miscella First Bed	
	Last Stra	Jordan Sandstone Depth to Bedrock 197 ft
	Located	
Remarks	Locate M	Digitization (Sereen) Wap (1.12,000) (> 13 meters)
M.G.S. NO. 146. GWQ NO. 0215.	System	UTM - NAD83, Zone 15, Meters X 510310 Y 4954139
		umber Verification Information from Input Date 01/22/2001
	Angled 1	rill Hole
	Well Co	
	Keys V	fell Co.     62012     KEYS WELL       e Business     Lic. or Reg. No.     Name of Driller
	Licens	Die. of Reg. 110. I Maine of Diffiel
Minnesota Well Index Report	206333	Printed on 03/26/2019

206333

County Quad

Quad ID

Dakota

87A

Hastings

MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING RECORD

Minnesota Statutes Chapter 1031

**Entry Date** 

**Received Date** 

12/27/1989

Update

07/11/2018

Well Name	Township	Range	Dir Secti	on Subs	ection	Use		Status	Well Depth	Depth Completed	Date Well Completed	Lic/Reg. No.
HASTINGS 3	115	17	W 28	BCA	CDD	community s	upply	A	299 ft.	299 ft.	09/20/1956	62012
Elevation 778 ft.	Elev. Method	7.5 r	ninute topogr	aphic map (+	-/- 5 feet)	Aquifer	Jordan		Depth to Bedrock	197 ft Open Hole	208 - 299 ft <b>Stat</b>	ic Water Level 67 ft
Field Located By	Minnesota D	Departmer	nt of		ocate Met		zation (Screen	) - Map (1:12	,000) (>15	Universal Trans	verse Mercator (UTM) - NAD	83 - Zone 15 -
Unique No. Verified	Information 1	from own	er-site	Iı	nput Sour	ce Minne	esota Departme	ent of Health		UTM Easting (X	510310	
Geological Interpretation	Bru	ce Bloom	ngren	Iı	nput Date	01/22/	2001			UTM Northing		
Agency (Interpretation)										Interpretaion M	dethod Geologic study	y 1:24k to 1:100k
				Dep	oth (ft.)		Eleva	tion (ft.)				
Geological Material	Co	olor	Hardness	From	To	Thickness	From	To	Stratigraphy	Primary Lithology	Secondary	Minor Lithology
CLAY				0	9	9	778	769	clay	clay		
SAND & GRAVEL				9	79	70	769	699	sand +larger	sand	gravel	
SAND & CLAY				79	103	24	699	675	clay+sand	sand	clay	
HARDPAN				103	107	4	675	671	pebbly sand/silt/clay	hardpan		
CLAY	BI	LUE		107	137	30	671	641	clay-gray	clay		
HARDPAN				137	169	32	641	609	pebbly sand/silt/clay	hardpan		
CLAY	BI	LUE		169	176	7	609	602	clay-gray	clay		
HARDPAN				176	197	21	602	581	pebbly sand/silt/clay	hardpan		
SANDROCK (JORDAN	1)			197	267	70	581	511	Jordan Sandstone	sandstone		
SANDSTONE	GI	RAY		267	299	32	511	479	Jordan Sandstone	sandstone		
Minnesota Well	l Index -	Strati	graphy	Report	t			2063	333			Printed on 03/26/2019

207993

County DakotaQuad VermillionQuad ID 87B

## MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

**Entry Date** 

12/27/1989

HE-01205-15

**Update Date** 10/04/2018

Well Name Township	Range	Dir Section			Well Depth		<b>Depth Completed</b>		ell Completed	
HASTINGS 4 115	17	W 32	DABBBA		400 ft.		400 ft.	08/30/19	961	
Elevation 863 ft. Elev. Mo	ethod	7.5 minute topog	graphic map (+	/- 5 feet)	Drill Method	Cable To	ol	Drill Fluid		
Address					Use comm	unity supply	(municipal)		Status	Active
Contact HASTINGS	MN 55033	3			Well Hydrofra	actured?	Yes No	From	To	
Well HASTINGS	MN 55033	3			Casing Type	Step do		 Joint		
Stratigraphy Information					Drive Shoe?	Yes	No	Above/Below		
Geological Material	From	To (ft.) C	Color I	Hardness	Casing Diame	eter W	eight		Hole Diamete	er
SAND & GRAVEL	0	36			16 in. To	312 ft.	lbs./ft.		24 in. To	400 ft.
SANDY YELLOW CLAY	36	56			24 in. To	58 ft.	lbs./ft.			
LIMESTONE & SHALE	56	70								
LIMESTONE & SHALE-	70	124								
LIMESTONE & SOME	124	165			Open Hole	Erom	214 ft	To 400	ft	
LIMESTONE, SHALE &	165	180			Screen?	From	314 ft. <b>Type</b>	To 400 Make	ft.	
LIMESTONE & SHALE	180	235			Sereem.					
LIMESTONE, SHALE-	235	260								
LIMESTONE, SHALE-	260	290								
LIMESTONE &	290	295			Static Water	Level				
SANDSTONE	295	305			138 ft.	land surf	ace	Measure	08/30/1961	
SANDSTONE	305		ELLOW		D	1 (11 1-				
SANDSTONE & SHALE	341			HARD	Pumping Le			600		
SANDSTONE	360		ELLOW		162 ft.	hrs.	Pumping at	600 g	.p.m.	
SANDSTONE	385		SRAY		Wellhead Co					
SHALE	398	400			Pitless adapter				lodel	
						Protection	i⊥ 12 ir ental Wells and Bo	n. above grade		
					Grouting Inf		Well Grouted?	Yes N	o Not S	Specified
					Material	.01111111011		ount		o To
					neat cement		Alli	ount	0 ft. 3	
					neat coment				0 11. 3	14 16.
					Nearest Kno	own Source	of Contamination			
					fe	eet	Direction			Type
					Well disinfe	ected upon co	ompletion?	Yes	No	
					Pump Manufacturer		t Installed D	ate Installed		
					Model Numb	er	HP	<u>0</u> Vo	lt	
					Length of dro	p pipe	ft Capacity	g.p.	Тур	
					Abandoned					
					Does property	y have any not	in use and not sealed	well(s)?	Yes	No
					Variance				_	
					Was a varian	ce granted fror	n the MDH for this we	ell?	Yes	No
					Miscellaneo					
					First Bedrock		Ou Chien Group	Aquifer		
					Last Strat Located by		ence Formation	Depth to Be	drock 56	ft
Remarks					Locate Metho		nesota Department tization (Screen) - 1		15 matara)	
COUNTRY ESTATES BLK 5 LOT	1.				System	2.8.	D83, Zone 15, Meters			52284
16" LINEAR PRESSURE GROUTE	ED FROM I	BOTTOM TO SU	RFACE WITH	H 1:1	"	er Verification		5070		/22/2001
SAND-CEMENT READY MIX. DIAMETER OF OPEN HOL	E IN ROCE	K, 24", EXTENDI	ING FROM BO	OTTOM OF	Angled Drill	Hole				
16:, TO BOTTOM OF HOLE AT 400'. SAN	ND CONTE	NT AT GOOGDM	AFTED							
DEVELOPMENT, 2 PPM.	1D CONTE	411 AT 2000FM	MILEK							
					Well Contra	eter				
					Tri-state W			27118	BENEK	FR
					Licensee B		Lic.	or Reg. No.	Name of D	
								5		
				20'	7993				D. C. C.	02/26/2010
Minnesota Well Index	Repor	<b>·t</b>			<del>-</del>				Printed	on 03/26/2019

207993

County

Dakota

Quad Quad ID

Vermillion 87B

WELL AND BORING RECORD

Minnesota Statutes Chapter 1031

MINNESOTA DEPARTMENT OF HEALTH

**Entry Date** 

12/27/1989

Update

**Received Date** 

10/04/2018

Well Name	Township	Range	Dir Section	Subsec	ction	Use		Status	Well Depth	Depth Completed	Date Well Completed	Li	c/Reg. No.	
HASTINGS 4	115	17	W 32	DABI	BBA	community su	ipply	A	400 ft.	400 ft.	08/30/1961	27	118	
Elevation 863 ft.	Elev. Method	7.5 n	ninute topograph	ic map (+/-	- 5 feet)	Aquifer	Jordan		Depth to Bedrock	56 ft Open Hole	314 - 400 ft <b>St</b>	atic Water Level	138	
Field Located By Unique No. Verified Geological Interpretation Agency (Interpretation)	Minnesota D Information Bru		er-site	Inj	cate Meth put Source put Date	Digitiz	ation (Screen sota Departm 2001		. , ,	Universal Transver UTM Easting (X) UTM Northing (Y) Interpretaion Meth		<b>D83 - Zone 15 -</b> dy 1:24k to 1:100	K	
				Dept	h (ft.)		Eleva	tion (ft.)						_
Geological Material	Co	olor	Hardness	From	To	Thickness	From	To	Stratigraphy	Primary Lithology	Secondary	Minor Li	thology	
SAND & GRAVEL				0	36	36	863	827	sand +larger	sand	gravel			
SANDY YELLOW CLA	AY			36	56	20	827	807	clay+sand-yellow	clay	sand			
LIMESTONE & SHALE	Е			56	70	14	807	793	Prairie Du Chien	dolomite				
LIMESTONE & SHALE	E-TRACE			70	124	54	793	739	Prairie Du Chien	dolomite				
LIMESTONE & SOME	SHALE			124	165	41	739	698	Prairie Du Chien	dolomite				
LIMESTONE, SHALE &	&			165	180	15	698	683	Prairie Du Chien	dolomite				
LIMESTONE & SHALE	Е			180	235	55	683	628	Prairie Du Chien	dolomite				
LIMESTONE, SHALE-				235	260	25	628	603	Prairie Du Chien	dolomite				
LIMESTONE, SHALE-				260	290	30	603	573	Prairie Du Chien	dolomite				
LIMESTONE & SANDS	STONE			290	295	5	573	568	Jordan Sandstone	sandstone	dolomite			
SANDSTONE				295	305	10	568	558	Jordan Sandstone	sandstone				
SANDSTONE	Y	ELLOW		305	341	36	558	522	Jordan Sandstone	sandstone				
SANDSTONE & SHAL	E G	RAY	HARD	341	360	19	522	503	Jordan Sandstone	sandstone	shale			
SANDSTONE	Y	ELLOW		360	385	25	503	478	Jordan Sandstone	sandstone				
SANDSTONE	G	RAY		385	398	13	478	465	Jordan Sandstone	sandstone				
SHALE				398	400	2	465	463	St.Lawrence	shale				
														_
Minnesota Well	l Index -	Strati	graphy R	eport				2079	993			Printe	ed on 03/2	26/

207639

County DakotaQuad VermillionQuad ID 87B

## MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

Entry Date Update Date 12/27/1989 11/28/2018

HE-01205-15

Well Name Townsh HASTINGS 5 115	ip Range 17	Dir Section W 29	ACDDCD		Well Depth 356 ft.		Depth Completed 355 ft.	Date V 09/04/2	<b>Vell Completed</b> 1970	l
Elevation 860 ft. Elev.			graphic map (+/- 5		Drill Method	Cable Too		Drill Fluid		
Address					Use comm	unity supply	(municipal)		Status	Active
Well 55 HY HA	ASTINGS MN	55033			Well Hydrofra	actured?	Yes No	From	То	
	GS MN 55033				Casing Type	Step do		Joint	10	
Stratigraphy Information					Drive Shoe?	· —	No	Above/Below	0 ft.	
Geological Material	From	To (ft.)	Color Har	dness	Casing Diame	eter W	eight		Hole Diamete	er
SAND & CLAY	0	8			24 in. To	277 ft.	lbs./ft.		29 in. To	356 ft.
SHAKOPEE	8	264			30 in. To	26 ft.	lbs./ft.			
JORDAN	264	276								
JORDAN	276	353								
SANDROCK AND	353	355			Open Hole	From	277 ft.	To 350	6 ft.	
SHALE	355	356		-	Screen?		Type	Make	. II.	
					Static Water 147 ft.	Level	ace	Measure	09/04/1970	
					Pumping Le	vel (below la	and surface)			
					241 ft.	hrs.	Pumping at	1800	g.p.m.	
					Wellhead Co	_				
						r manufacturer			Model	
						Protection le (Environm	ental Wells and Bo	n. above grade orings ONLY)		
					Grouting Inf		Well Grouted?		No Not S	Specified
					Material neat cement		Am 33	Cubic yards	From T 0 ft. 2	o 77 ft.
					fe	own Source of the control of the con	of Contamination Direction ompletion?	Yes	No	Туре
					Pump Manufacturer Model Numbe	r's name		Date Installed $\underline{0}$ V	olt	
					Length of dro		ft Capacity		Тур	
					Abandoned					
					Does property	y have any not	in use and not sealed	well(s)?	Yes	No
					Variance	<u></u>				
							n the MDH for this w	ell?	Yes	∐ No
					Miscellaneou First Bedrock Last Strat Located by	Prairie D St.Lawre	Ou Chien Group ence Formation nesota Department	Depth to B	Jordan edrock 8	ft
Remarks					Locate Metho	2.6.	tization (Screen) -			
M.G.S. NO. 583. GAMMA LOGGED 11-13-2018	R BY IIM TRAE	N			System		D83, Zone 15, Meter	207		53935
					Angled Drill	per Verification	1 Informati	on from	Input Date 01	1/22/2001
					angica Dilli					
					Well Contra					
					Keys Well		т.	62012	O'BRIE	
					Licensee B	usiness	Lic.	or Reg. No.	Name of D	miller
Minnesota Well Ind	lex Repor	t		207	639				Printed	on 03/26/2019

207639

County Quad

Quad ID

Dakota

87B

Vermillion

WELL AND BORING RECORD

Minnesota Statutes Chapter 1031

MINNESOTA DEPARTMENT OF HEALTH

**Entry Date** 

12/27/1989

Update

Received Date 11/28/2018

Well Name	Township	Range	Dir Sect	ion Subs	ection	Use		Status	Well Depth	Depth Completed	Date Well Completed	Li	c/Reg. No.	
HASTINGS 5	115	17	W 29	ACE	DDCD	community s	upply	A	356 ft.	355 ft.	09/04/1970	62	2012	
Elevation 860 ft.	Elev. Method	7.5 m	ninute topog	raphic map (+	-/- 5 feet)	Aquifer	Jordan		Depth to Bedrock	8 ft Open Hole	277 - 356 ft	Static Water Level	147	
Field Located By	Minnesota D	epartmen	t of	L	ocate Meth	od Digitiz	zation (Screen	ı) - Map (1:12	,000) (>15	Universal Transv	erse Mercator (UTM) - N	NAD83 - Zone 15 -		
Unique No. Verified	Information	from own	er-site	Iı	nput Sourc	e Minne	sota Departm	ent of Health		UTM Easting (X)	509532			
Geological Interpretation	Bru	ce Bloom	gren	I	nput Date	01/22/	2001			UTM Northing (Y	495393			
Agency (Interpretation)										Interpretaion Me	thod Cuttings +	geophysical log		
				Dep	oth (ft.)		Eleva	ntion (ft.)						_
Geological Material	Co	olor	Hardness	From	To	Thickness	From	To	Stratigraphy	Primary Lithology	Secondary	Minor Li	thology	
SAND & CLAY				0	8	8	860	852	clay+sand	sand	clay			
SHAKOPEE				8	264	256	852	596	Prairie Du Chien	dolomite				
JORDAN				264	276	12	596	584	Prairie Du Chien	dolomite				
JORDAN				276	353	77	584	507	Jordan Sandstone	sandstone				
SANDROCK AND SHA	LE			353	355	2	507	505	St.Lawrence	siltstone	shale	sandston	e	
SHALE				355	356	1	505	504	St.Lawrence	siltstone	shale			
								•	<b></b>					_
Minnesota Well	Index -	Stratis	graphy	Report	t			2076	39			Printe	ed on 03/2	26/2

207643

County DakotaQuad HastingsQuad ID 87A

## MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

Entry Date Update Date 12/27/1989 07/12/2018

HE-01205-15

Well Name	Township	Range	Dir Section	Subsection	Well Depth		pth Completed		ell Completed	l
HASTINGS 6	115	17	W 34	CDDBBA	332 ft.		2 ft.	02/28/1	972	
	ft. Elev. Me	thod	7.5 minute topogr	aphic map (+/- 5 feet)	Drill Method	Cable Tool		Drill Fluid		
Address					Use comm	nunity supply(mu	ınicipal)		Status	Active
Well	316 HY HAS	TINGS MI	N 55033		Well Hydrofra	actured?	Yes No	From	To	
Contact	HASTINGS N	MN 55033			Casing Type			Joint		
Stratigraphy Info			FF (6) G		Drive Shoe?		No	Above/Below	1 ft.	
Geological Materi	al	From 0	To (ft.) Co	olor Hardness	Casing Diam	_			Hole Diamet	
SAND & CLAY SAND		8	8 33		24 in. To	240 ft.	lbs./ft.		23 in. To	332 ft.
GRAVEL		33	40		30 in. To	98 ft.	lbs./ft.			
SAND		40	64							
GRAVEL AND L	IME	64	84							
LIME AND SAN		84	93		Open Hole	From 24		To 332	ft.	
LIME AND SAN		93	102		Screen?	T	Гуре	Make		
SHAKOPEE LIM	Е	102	229							
JORDAN SANDS	TONE	229	330							
JORDAN SANDS	TONE	330	332		Static Water	r I ovol				
					125 ft.	land surface	;	Measure	02/28/1972	
					Pumping Le	evel (below land	surface)			
					207 ft.	hrs. I	Pumping at	1200 g	g.p.m.	
					Wellhead C	ompletion				
						r manufacturer		N	Iodel	
					Casing At-grad	Protection de (Environment	X 12 in al Wells and Bor	. above grade rings ONLY)		
					Grouting In	formation	Well Grouted?	X Yes N	lo Not S	Specified
					Material		Amo	ount	From 7	Го
					neat cement		0	Sacks	0 ft. 2	40 ft.
					fe	own Source of C eet ected upon comp	Direction	Yes	□ No	Туре
					Pump Manufacture	Not Ins	stalled Da	ate Installed		
					Model Numb	er	HP (	<u>)</u> Vo	olt	
					Length of dro	op pipe	ft Capacity	g.p.	Typ	
					Abandoned					
						y have any not in u	use and not sealed v	well(s)?	Yes	No
					Variance	. 16 . 4	MDHC 4:	110	Vac	
							e MDH for this we	:117 [	Yes	∐ No
					Miscellaneo First Bedrock Last Strat Located by	Prairie Du C St.Lawrence	Chien Group e Formation	Aquifer Depth to Be		ft
Remarks					Located by Locate Metho		sota Department	от неани Мар (1:12,000) (:	>15 meters)	
M.G.S. NO. 750.					System		3, Zone 15, Meters			51677
BAILED 170 YDS.	SANDSTONE.	DYNAMIT	E 250 LBS.		Unique Numb	ber Verification	Informatio	on from I	nput Date 01	1/22/2001
					Angled Dril	l Hole				
					Well Contra					
					Keys Well Licensee F		Lic.	62012 or Reg. No.	O'BRIE Name of I	
Minnesota V	Vell Index	Repor	t	20	7643				Printed	on 03/26/2019

207643

County
Quad
Quad ID

Dakota

Hastings 87A

WELL AND BORING RECORD

Minnesota Statutes Chapter 1031

MINNESOTA DEPARTMENT OF HEALTH

**Entry Date** 

12/27/1989

Update

Received Date	07/12/2018

Well Name	Township	Range	Dir Section	Subse	ction	Use		Status	Well Depth	Depth Completed	Date Well Completed	Lic/Reg. No.	
HASTINGS 6	115	17	W 34	CDD	BBA	community su	ipply	A	332 ft.	332 ft.	02/28/1972	62012	
Elevation 835 ft.	Elev. Method	7.5 n	ninute topograph	ic map (+/	- 5 feet)	Aquifer	Jordan		Depth to Bedrock	93 ft Open Hole	240 - 332 ft	Static Water Level 125	ft
Field Located By	Minnesota I	Departmen	nt of	Lo	cate Metl	nod Digitiz	ation (Screen)	) - Map (1:12	2,000) (>15	Universal Transv	erse Mercator (UTM) -	NAD83 - Zone 15 -	
Unique No. Verified	Information	from own	er-site	In	put Sourc	e Minne	sota Departme	ent of Health		UTM Easting (X)	512270		
Geological Interpretation	Bru	ice Bloom	igren	In	put Date	01/22/2	2001			UTM Northing (Y			
Agency (Interpretation)										Interpretaion Me	thod Geologic	study 1:24k to 1:100k	
				Dept	th (ft.)		Eleva	tion (ft.)					
Geological Material	C	olor	Hardness	From	To	Thickness	From	To	Stratigraphy	<b>Primary Lithology</b>	Secondary	Minor Lithology	
SAND & CLAY				0	8	8	835	827	clay+sand	sand	clay		
SAND				8	33	25	827	802	sand	sand			
GRAVEL				33	40	7	802	795	gravel (+larger)	gravel			
SAND				40	64	24	795	771	sand	sand			
GRAVEL AND LIME O	CHUNKS			64	84	20	771	751	gravel (+larger)	gravel	cobble		
LIME AND SAND				84	93	9	751	742	sand +larger	cobble	sand		
LIME AND SAND				93	102	9	742	733	Prairie Du Chien	dolomite			
SHAKOPEE LIME				102	229	127	733	606	Prairie Du Chien	dolomite			
JORDAN SANDSTON	Е			229	330	101	606	505	Jordan Sandstone	sandstone			
JORDAN SANDSTON	Е			330	332	2	505	503	St.Lawrence	siltstone	shale		
		<b>G</b> 4 4•	, ~					2070	5/12				
Minnesota Wel	ı ındex -	Strati	grapny R	eport				<b>4</b> 0/0	J <del>1</del> J			Printed on 03/2	26/2019

509053

Minnesota Well Index Report

County Dakota Quad Hastings Quad ID 87A

#### MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

**Entry Date Update Date**  03/01/2002 07/12/2018

Printed on 03/26/2019

HE-01205-15

Well Name Township	Range Dir	Section Subsec	tion	Well Depth	Depth Completed	Date W	ell Completed
HASTINGS 7 115	17 W	28 DABD	СВ	285 ft.	285 ft.	10/09/19	989
Elevation 784 ft. Elev. Met	t <b>hod</b> LiDAR	1m DEM (MNDNR	)	Drill Method Cable	Tool	Drill Fluid	
Address				Use community sup	oply(municipal)		Status Active
Well ASHLAND S'	T HASTINGS M	IN 55033		Well Hydrofractured?	Yes No	From	То
Contact 100 SIBLEY S	ST HASTINGS I	MN 55033		Casing Type Step	o down	Joint	Welded
Stratigraphy Information				Drive Shoe? Yes	No	Above/Below	2 ft.
Geological Material		(ft.) Color	Hardness	Casing Diameter	Weight		Hole Diameter
SAND AND GRAVEL	0 56	BROWN	SOFT	24 in. To 205 ft	t. 94.6 lbs./ft.		29 in. To 205 ft.
LIMEROCK	56 57	TAN	HARD	30 in. To 63 ft	t. 118. lbs./ft.		23 in. To 285 ft.
SAND	57 59	BROWN	SOFT				
LIMEROCK (BROKEN) LIMEROCK (HARD)	59 62 62 65	TAN TAN	MEDIUM HARD				
SAND	65 66	BROWN	SOFT	Open Hole Fron	n 205 ft.	To 285	ft.
LIMEROCK	66 75	TAN	HARD	Screen?	Type	Make	
SANDSTONE	75 78	TAN	MEDIUM				
LIMEROCK	78 195		HARD				
SANDROCK	195 283	TAN	MEDIUM	Static Water Level			
LIMEROCK	283 285	GRAY	HARD		surface	Measure	10/04/1989
				Pumping Level (belo	w land surface)		
				123 ft. 2 h	rrs. Pumping at	1000 g.	.p.m.
				Wellhead Completio	n		
				Pitless adapter manufact			lodel
				Casing Protectio	on <b>X</b> 12 in onmental Wells and Bor	above grade	
				Grouting Informatio		X Yes No	o Not Specified
				Material	Amo		From To
				neat cement	66	Cubic yards	0 ft. 205 ft.
				feet	rce of Contamination Direction		Туре
				Well disinfected upo Pump	Not Installed Da	Yes [ate Installed	No 04/00/1990
				Manufacturer's name	PEERLESS	160 11	1, 460
				Model Number Length of drop pipe	HP <u>4</u> 220 ft Capacity	460 Vol 1200 g.p.	lt <u>460</u> Typ Turbine
				Abandoned	<u>220</u> It capacity	<u>1200</u> g.p.	Typ <u>Turbine</u>
					not in use and not sealed v	well(s)?	Yes X No
				Variance Was a variance granted	from the MDH for this we	11?	Yes No
				Miscellaneous			
				Last Strat St.La	rie Du Chien Group awrence Formation	Aquifer Depth to Bed	
Remarks					Minnesota Department of Digitization (Screen) - M		-15 meters)
TOTAL PUMP HOURS: 51 HRS.	BLATED 150# DY	YNAMITE AND BA	LED OUT.		- NAD83, Zone 15, Meters		
260 YDS AND LOOSE SANDROCH	K AND AIR.			Unique Number Verific	cation Info/GPS	from data In	put Date 01/22/2001
DEVELOPMENT 23 HOURS. 1ST TEST - (BEFORE DEVELOPM 935 GPM 78-6FT DD. (3IN/16 SANI				Angled Drill Hole			
M.G.S. NO. 2968. LOGGED GEOSPHERE MIDWEST	11/12/91			Well Contractor			
POOGED GEORI HEKE MID MEST	11/14/71			Keys Well Co.		62012	RUSSELL, J.
				Licensee Business	Lic.	or Reg. No.	Name of Driller
			=	0.52			
<b>.</b>	<b>D</b>		509	0053			Printed on 03/26/2010

509053

County Quad

Quad ID

Dakota

Hastings 87A

## MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING RECORD

Minnesota Statutes Chapter 1031

**Entry Date** 

**Received Date** 

03/01/2002

Update

07/12/2018

	Township 115	Range 17	Dir Section W 28	Subsect DABI		Use community su	ınnly	Status A	Well Depth 285 ft.	<b>Dept</b> 285 1		npleted		O/09/		mplet	æd			c/ <b>Reg. No.</b> 2012	
Elevation 784 ft.	Elev. Method	LiDA	AR 1m DEM (MI	NDNR)		Aquifer	Jordan		Depth to Bedrock	59	ft	Open Hole	e	205	- 28	5 f	ft	Static Water	Level	84	ft
Field Located By Unique No. Verified Geological Interpretation Agency (Interpretation)	Minnesota D Info/GPS fro John		ource	Inp	cate Meth out Source out Date	8	ation (Screen) sota Departmen 2001		,000) (>15		U	niversal Tra TM Easting TM Northin	g(X) ng(Y)		5 4	1133′ 9537:	7 5	NAD83 - Zono		-	
Agency (Interpretation)				Dept	h (ft.)		Elevati	ion (ft.)				nor promion				eoroș	31C S	<u>tudy 1.24k i</u>	1.100	<u> </u>	
Geological Material	Co	lor	Hardness	From	To	Thickness	From	To	Stratigraphy	P	rima	ry Lithology	7		Seco	ndary	y		Minor Li	thology	
SAND AND GRAVEL	ВІ	ROWN	SOFT	0	56	56	784	728	sand +larger	S	and				grav	el					
LIMEROCK	TA	AN	HARD	56	57	1	728	727	boulder or boulders	b	ould	er									
SAND	BI	ROWN	SOFT	57	59	2	727	725	sand	S	and										
LIMEROCK (BROKEN)	T) TA	AN	MEDIUM	59	62	3	725	722	Prairie Du Chien	d	olom	ite									
LIMEROCK (HARD)	TA	AN	HARD	62	65	3	722	719	Prairie Du Chien	d	olom	ite									
SAND	BI	ROWN	SOFT	65	66	1	719	718	Prairie Du Chien	S	andst	one									
LIMEROCK	TA	AN	HARD	66	75	9	718	709	Prairie Du Chien	d	olom	ite									
SANDSTONE	TA	AN	MEDIUM	75	78	3	709	706	Prairie Du Chien	S	andst	one									
LIMEROCK	TA	AN	HARD	78	195	117	706	589	Prairie Du Chien	d	olom	ite									
SANDROCK	TA	AN	MEDIUM	195	283	88	589	501	Jordan Sandstone	S	andst	one									
LIMEROCK	GI	RAY	HARD	283	285	2	501	499	St.Lawrence	d	lolom	iite			silts	tone					
Minnesota Well	l Index -	Strati	graphy R	eport				5090	)53										Print	ed on 03/2	26/201

686266

Minnesota Well Index Report

Dakota County Hastings Ouad Quad ID 87A

#### MINNESOTA DEPARTMENT OF HEALTH WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

**Entry Date Update Date** 

**Received Date** 

02/15/2006 07/12/2018 11/06/2006

HE-01205-15

Well Name Well Depth **Date Well Completed** Township Range Dir Section Subsection Depth Completed HASTINGS 8 17 W 34 **BDCDCA** 280 ft. 280 ft. 06/00/2006 115 Drill Fluid Water 7.5 minute topographic map (+/- 5 feet) Drill Method Elevation 785 ft. Elev. Method Cable Tool Address Use community supply(municipal) Status Active Well Well Hydrofractured? COMMERCE DR HASTINGS MN 55033 Yes No X From  $T_0$ 101 EAST 4TH ST HASTINGS MN 55033 Contact Casing Type Step down **Joint** Welded Drive Shoe? Yes X Stratigraphy Information No Above/Below 1 ft. Geological Material From To (ft.) Color Hardness Casing Diameter Weight **Hole Diameter** SOFT DRIFT 0 3 BLACK ft. 94.7 24 in To 188 lbs /ft 30 in. To 280 ft. LIMESTONE 3 178 YELLOW HARD 30 in. To ft. 118. lbs./ft. SANDSTONE 178 184 YELLOW **MEDIUM** SANDSTONE 184 273 YELLOW **MEDIUM** SHALE 273 280 **GRAY HARD** Open Hole То 280 From ft. ft. 188 Make Screen? Type Static Water Level 06/19/2006 land surface Measure Pumping Level (below land surface) 155 ft. 8 hrs. Pumping at 1200 g.p.m. Wellhead Completion Pitless adapter manufacturer Model X 12 in. above grade Casing Protection At-grade (Environmental Wells and Borings ONLY) Well Grouted? X Yes **Grouting Information** No Not Specified Material Amount From To ft. 188 neat cement 36.5 Cubic yards ft. Nearest Known Source of Contamination 150 Northeas Direction feet Body of water Type Well disinfected upon completion? X Yes Pump Date Installed Not Installed Manufacturer's name HP Model Number Volt Length of drop pipe Capacity g.p. Typ Abandoned Yes X No Does property have any not in use and not sealed well(s)? Variance Was a variance granted from the MDH for this well? X No Miscellaneous First Bedrock Prairie Du Chien Group Aquifer Jordan Last Strat St.Lawrence Formation Depth to Bedrock ft Located by Minnesota Department of Health GPS SA Off (averaged) (15 meters) Locate Method GAMMA LOGGED 6-28-2006. M.G.S. NO. 4658. LOGGED BY JIM TRAEN. UTM - NAD83, Zone 15, Meters System X 512174 Y 4952335 Unique Number Verification Input Date Info/GPS from data 01/26/2006 **Angled Drill Hole** Well Contractor Keys Well Drilling Co. 1347 ALLAN, J. Licensee Business Lic. or Reg. No. Name of Driller 686266 Printed on 03/26/2019

686266

County Quad

Quad ID

Dakota

Hastings

87A

WELL AND BORING RECORD

Minnesota Statutes Chapter 1031

MINNESOTA DEPARTMENT OF HEALTH

**Entry Date** 

02/15/2006

Update

11/06/2006

ate 07/12/2018

HASTING   Flee   Hasting	Well Name	Township	Range	Dir Section	Subse	ction	Use		Statu	6 Well Depth	Depth Completed	Date Well Completed	Lic/Reg. No.
Field Located By Unique No. Verified Geological Interpretation Agency (Interpretation)  Color Hardness From To Thickness From To Stratigraphy DRIFT BLACK SOFT BLACK SOFT SANDSTONE YELLOW MARD SANDSTONE YELLOW MEDIUM 178 184 6 607 601 Prairie Du Chien dolomite SANDSTONE SANDSTONE SHALE GRAY HARD STANDSTONE SHALE GRAY HARD STANDSTONE SHALE SANDSTONE SHALE GRAY HARD STANDSTONE SHALE SHALE STANDSTONE SHALE STANDSTONE SHALE SHA	HASTINGS 8	115	17	W 34	BDC	DCA	community s	upply	A	280 ft.	280 ft.	06/00/2006	1347
Unique No. Verified Geological Interpretation Agency (Interpretation)  To Stratigraphy DRIFT BLACK SOFT BLACK SOFT BANDSTONE SANDSTONE SANDSTONE SANDSTONE SANDSTONE SANDSTONE SANDSTONE SHALE GRAY HARD SANDSTONE SHALE SHALE SANDSTONE SHALE SHALE SANDSTONE	Elevation 785 ft.	Elev. Method	7.5 n	ninute topograpl	nic map (+/	- 5 feet)	Aquifer	Jordan		Depth to Bedrock	3 ft Open Hole	188 - 280 ft <b>Static</b>	Water Level 90
Geological Interpretation  Agency (Interpretation)  The put Date 101/26/2006  Thickness From To Stratigraphy Primary Lithology Secondary Minor Lithology  DRIFT BLACK SOFT 0 3 3 785 782 Recent deposit-black soil organic deposits  LIMESTONE YELLOW HARD 3 178 175 782 607 Prairie Du Chien dolomite  SANDSTONE YELLOW MEDIUM 178 184 6 607 601 Prairie Du Chien dolomite  SANDSTONE YELLOW MEDIUM 184 273 89 601 512 Jordan Sandstone  SHALE GRAY HARD 273 280 7 512 505 St.Lawrence siltstone dolomite	Field Located By						or or or	SA Off (averag	ged) (15 met	ers)	Universal Trans	verse Mercator (UTM) - NAD83	- Zone 15 -
Agency (Interpretation)  The pth (ft.)  Seological Material  Color  Hardness From To Thickness From To Stratigraphy Primary Lithology Organic deposits  Organic deposits  From To Thickness From To Stratigraphy Primary Lithology Organic deposits  Organic deposits  From To Thickness From To Stratigraphy Primary Lithology Organic deposits  Organic deposits  Organic deposits  From To Thickness From To Thicknes	Unique No. Verified	Info/GPS fro	m data so	ource	In	put Sourc	e Minne	esota Departm	ent of Health	1	UTM Easting (X	512174	
Geological Material Color Hardness From To Thickness From To Stratigraphy Primary Lithology Secondary Minor Lithology  DRIFT BLACK SOFT 0 3 3 785 782 Recent deposit-black soil organic deposits  LIMESTONE YELLOW HARD 3 178 175 782 607 Prairie Du Chien dolomite  SANDSTONE YELLOW MEDIUM 178 184 6 607 601 Prairie Du Chien dolomite  SANDSTONE YELLOW MEDIUM 184 273 89 601 512 Jordan Sandstone  SHALE GRAY HARD 273 280 7 512 505 St. Lawrence siltstone dolomite	Geological Interpretation	John	n Mossler	•	In	put Date	01/26/	2006			UTM Northing (	<b>(Y)</b> 495233	
Geological MaterialColorHardnessFromToThicknessFromToStratigraphyPrimary LithologySecondaryMinor LithologyDRIFTBLACKSOFT033785782Recent deposit-blacksoilorganic depositsLIMESTONEYELLOWHARD3178175782607Prairie Du ChiendolomiteSANDSTONEYELLOWMEDIUM1781846607601Prairie Du ChiendolomiteSHALEGRAYHARD2732807512505St.Lawrencesiltstonedolomite	Agency (Interpretation)										Interpretaion M	<b>lethod</b> Inferred from ge	ophysical log
DRIFT BLACK SOFT 0 3 3 785 782 Recent deposit-black soil organic deposits  LIMESTONE YELLOW HARD 3 178 175 782 607 Prairie Du Chien dolomite  SANDSTONE YELLOW MEDIUM 178 184 6 607 601 Prairie Du Chien dolomite  SANDSTONE YELLOW MEDIUM 184 273 89 601 512 Jordan Sandstone sandstone  SHALE GRAY HARD 273 280 7 512 505 St. Lawrence siltstone dolomite					Dept	th (ft.)		Eleva	tion (ft.)				
LIMESTONE YELLOW HARD 3 178 175 782 607 Prairie Du Chien dolomite SANDSTONE YELLOW MEDIUM 178 184 6 607 601 Prairie Du Chien dolomite SANDSTONE YELLOW MEDIUM 184 273 89 601 512 Jordan Sandstone sandstone SHALE GRAY HARD 273 280 7 512 505 St.Lawrence siltstone dolomite	Geological Material	Co	olor	Hardness	From	To	Thickness	From	To	Stratigraphy	Primary Lithology	Secondary	Minor Lithology
SANDSTONE YELLOW MEDIUM 178 184 6 607 601 Prairie Du Chien dolomite SANDSTONE YELLOW MEDIUM 184 273 89 601 512 Jordan Sandstone sandstone SHALE GRAY HARD 273 280 7 512 505 St. Lawrence siltstone dolomite	DRIFT	BI	LACK	SOFT	0	3	3	785	782	Recent deposit-black	soil	organic deposits	
SANDSTONE YELLOW MEDIUM 184 273 89 601 512 Jordan Sandstone sandstone SHALE GRAY HARD 273 280 7 512 505 St.Lawrence siltstone dolomite	LIMESTONE	YI	ELLOW	HARD	3	178	175	782	607	Prairie Du Chien	dolomite		
SHALE GRAY HARD 273 280 7 512 505 St.Lawrence siltstone dolomite	SANDSTONE	YI	ELLOW	MEDIUM	178	184	6	607	601	Prairie Du Chien	dolomite		
	SANDSTONE	Y	ELLOW	MEDIUM	184	273	89	601	512	Jordan Sandstone	sandstone		
	SHALE	Gl	RAY	HARD	273	280	7	512	505	St.Lawrence	siltstone	dolomite	
										<u> </u>			
Minnesota Well Index - Stratigraphy Report 686266 Printed on 03/26	Minnesota Wel	l Index -	Strati	granhy R	Renort				686	266			Printed on 03/26/20

### Appendix B

**Aquifer Test Data and Analysis** 



# **Determination of Aquifer Properties and Aquifer Test Plan (DAP-ATP) Form**

Public Water Supply	7 <b>ID</b> :  119	0012 J	PWS Name: City	of Hastings		
Contact Information for Person Completing this Form						
Name: John Greer, PG						
a .l.1	Bar	Barr Engineering Co.				
Add	430	00 MarketPointe	Drive, Suite 20	0		
City, State,	, zip: Min	neapolis, MN 5	5435			
Phone, Fax, e-r	mail: 952	2-832-2691 (pho	one) 952-832-20	601 (fax)		
	Aquit	fer Properties D	etermination M	lethods		
For Methods 1 - 5, ch	neck all tha	t apply - attach Su	mmary of Aquifer I	Properties Based o	n Existing Data	
		=	irements of wellhead ected to the public v	-		
	iously condu	ucted on another we	irements of wellhead Ill in a hydrogeologic	•		
3. 4720.5520 an	An existing pumping test that does not meet the requirements of wellhead protection rule part  3. 4720.5520 and that was previously conducted on: 1) a public water supply well or 2) another well in a hydrogeologic setting determined by the department to be equivalent.					
			the public water sup etting determined by			
4. conducted on other wells in a hydrogeologic setting determined by the department to be equivalent.  5. An existing published transmissivity value.						
For Method 6 or 7 - attach detailed Aquifer Test Plan for Proposed Test						
6. system and th	at meets th	e conducted on a new or existing well connected to the public water supply e requirements for larger-sized water systems (wellhead protection rule part n must be approved before conducting the test.				
7. A proposed new test to be conducted on a new or existing public well connected to the public water supply system and that meets the requirements for smaller-sized water systems (wellhead protection rule part 4720.5530). The test plan must be approved before conducting the test.					-	
List the unique number of each public water supply well to which this DAP-ATP Form applies						
206333 (Well 3) 509053 (Well						
207993 (Well 4) 686266 (Well 8						
207639 (Well 5)						
207643 (Well 6)						
Submitted by: John G	reer	Prof. License: PG #30347		Date: 4/22/2019		
Reviewed by: Amal Djerrari		Approved: • Yes No		<b>Approval Date: </b> 4/23/2019		

Summary of Aquifer Properties Based on Existing Data							
Aquifer Name: Jordan Sandstone	Aquifer Code: CJDN						
Hydraulic Confinement Confined Unconfined	Fractured Rock						
Aquifer Test Number of test(s) on file used to compile the information tabulated below:							
Hastings Well 5 test (October 2001)							
Aquifer Properties Summary Table							

Aquiter Properties Summary Table					
Donnes entative Val	l lmia	Raı	. / 0/		
Representative Val	ues Unit		Minimum	Maximum	+/- %
Top Stratigraphic Elev.	579.3	feet (MSL)	573	584	+0.8/-1
Bottom Stratigraphic Elev.	483.6	feet (MSL)	465	507	+5/-4
Transmissivity (T)	5,444	ft <sup>2</sup> /day	1,549	20,580	+278/-72
Aquifer Thickness (b)	95.7	feet	77	108	+13/-20
Saturated Thickness* (b)		feet			
Hydraulic Conductivity (k)	56.9	ft/day	20.1	191	+850/-183
Primary Porosity (e <sub>p</sub> )	20	0.00 %			
Secondary Porosity** (e <sub>s</sub> )		0.00 %			
Storativity (S)	6.87e-5	dimensionless	3.33e-5	1.21e-4	+76/-52
Characteristic Leakage (L)		feet			
Hydraulic Resistance (c)		days			

Notes: Shaded fields are required - \* hydraulically unconfined aquifer - \*\* dual porosity aquifer because of fractures or solution weathering

#### Describe rationale for selected method(s). Attach documentation and analysis.

The test was conducted from October 23, 2001 through October 29, 2001. Well 5 (207639) was the pumping well and Wells 3 (20633) and 4 (207993) were used as observation wells. Wells 6 and 7 were periodically pumped during the test.

Test results were used for the previous updates of the Hastings WHPP.

Measured transmissivity ranged from 143.9 m\*\*2/day (1,549 ft\*\*2/day) to 1,912 m\*\*2/day (20,580 ft\*\*2/day). The geometric mean of 505.8 m\*\*2/day (5,444 ft\*\*2/day) was selected as the representative value for the Jordan.

Jordan thickness is 102 feet (31.1 m) at Well 3, 108 ft (32.9 m) at Well 4, and 77 feet (23.5 m) at Well 5. The average thickness is 95.7 feet (29.2 m).

Using the representative T value and average aquifer thickness gives a representative K value of 56.9 ft/day (17.3 m/day). For the model sensitivity analysis, lower and upper bounds of 20.1 ft/day (6.1 m/day) and 191 ft/day (58.1 m/day) were calculated from the upper and lower bounds on transmissivity and aquifer thickness.

The Barr report on analysis of the pumping test data is attached.

# Appendix A City of Hastings Aquifer Test Report

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An aquifer test was performed in the Jordan Sandstone aquifer from October 23, 2001 through October 29, 2001 using City of Hastings Well 3 (unique number 206333), City of Hastings Well 4 (unique number 207993), and City of Hastings Well 5 (unique number 207639) (Figure A-1). Well construction is summarized on Table A-1 and the well records are presented in Appendix A-1. The aquifer thickness used in analysis of the aquifer test data (94 feet) was based on the formation picks from the well logs (see Table A-1).

The layout of the wells used in the test is shown on Figure A-1. Well 5 was the pumping well for this test and Wells 3 and 4 were used as observation wells.

As planned, a two-day background period preceded the 24-hour pumping period. Per the test plan, a recovery period followed the pumping period. Wells 3 and 4 did not pump at all during the entire test period. A copy of the approved pumping test plan is presented in Appendix A-2.

The test plan called for pressure transducers connected to Hermit data loggers to be installed in Wells 3 and 5. Due to wellhead configuration, it was not possible to place a transducer in Well 5. As attempt was made to record water levels in Well 5 by connecting the City's pressure transducer in that well to a Hermit data logger. Data recorded using the City's transducer could not be correlated with manual water level measurements made in the well. Since the water level data recorded using the City's transducer could not be verified the data were not used. Water levels were measured manually in Wells 4 and 5 periodically during the pumping and recovery periods of the test. Hydrographs for the monitored wells are shown on Figures A-2 through A-4.

Hastings Well 1 (unique number 207821) (Figure A-1) is completed in the Franconia-Ironton-Galesville aquifer. The other Hastings wells are completed in the Jordan Sandstone. No aquifer test was performed in the Franconia-Ironton-Galesville aquifer because the City of Hastings intends to abandon Well 1 before the end of 2002.

#### 2.0 Test Procedures

Pumping rates, volumes, and run times of the Hastings municipal wells during the aquifer test period were measured and recorded by the City's SCADA system (Appendix A-3). Total flow readings for Well 5 were also manually recorded from the totalizing flow meter at the wellhead during the pumping period of the test (Appendix A-4). Pumping of the City's wells during the aquifer test is summarized in Table A-2.

Water levels in Well 3were measured automatically using a Hermit 3000 data logger and a pressure transducer manufactured by In Situ, Inc. As noted above, water levels in Wells 4 and 5 were measured manually periodically during the pumping and recovery periods of the test. Water level data for the aquifer test are included on the compact disk attached to the main report (see Table 2 of the main report). Copies of the field data sheets from the aquifer test are presented in Appendix A-4.

In addition to water levels in Well 3, barometric pressure in Hastings during the aquifer test period was recorded using the Hermit 3000 data logger. The Hermit 3000 has an internal pressure transducer for measuring barometric pressure. Barometric pressure readings were taken throughout the test period at the same frequency as the water level measurements in Well 3.

Prior to analyzing the aquifer test data, the water level and barometric pressure data recorded at Well 3 were evaluated to determine if there was any correlation between changes in water levels in the well and changes in barometric pressure. Water level measured in a well open to a confined aquifer will fluctuate with changes in barometric pressure. These fluctuations in water level may be large enough to measure. The change in water level relative to the change in barometric pressure is called the barometric efficiency (e.g., Walton, 1987; Kruseman and de Ridder, 1991) and is expressed as a percentage of the change in barometric pressure when the barometric pressure is expressed in the same units as the water levels (e.g., feet or meters of water). If present, such a correlation must be filtered out of the water level data prior to data analysis.

Data from the background (i.e., prior to initiation of pumping in Well 5) and recovery periods of the test were used to try and determine a correlation between water level changes in Well 3 and changes in barometric pressure. Barometric pressures and water levels recorded at Well 3 are shown on Figure A-2. It appears that there were measurable water level fluctuations in Well 3 due to pumping in other City of Hastings wells during the background and recovery periods. These fluctuations were larger than the magnitude of potential water level changes due to barometric pressure changes. Thus, no correlation between changes in water level in Well 3 and changes in barometric pressure could be determined.

The pumping test data were analyzed with the software AQTESOLV for Windows (Duffield, 2000) using the Neuman-Witherspoon method (1969) for layered aquifers. This analysis assumes the aquifer is a layered, leaky system and that pumping is from one of the layers. Effects of leakage from the unpumped layer and release of water from the unpumped layer are included in the analysis. In the vicinity of the City of Hastings wells used for this test, the pumped layer is the Jordan Sandstone, the confining layer is the Oneota Dolomite (where present) and the unpumped layer is the upper part of the Prairie du Chien Group (where present) and overlying unconsolidated units. Well 3 appears to be located on the western side of a buried tributary bedrock valley. According to the Dakota County Geologic Atlas (Balaban and Hobbs, 1990), this tributary valley trends approximately north-south and the Jordan Sandstone subcrops in the center of this valley.

As described above, Hastings Well 5 was the pumping well for this aquifer test. In order to meet water demand during the test period, Hastings Wells 6 and 7 were pumped periodically during the aquifer test period. AQTESOLV is able to account for multiple pumping wells in the data analysis.

Data for the pumping and recovery periods for each well were combined in the analysis using the Neuman-Witherspoon (see Figures A-5 through A-7). As indicated in Table A-3, the transmissivities determined using the Neuman-Witherspoon method varied by less than a factor of 3. This suggests that the aquifer properties are approximately uniform over the area affected by the aquifer test.

Recovery period data from each well were also analyzed separately using the Theis (1935) recovery method in AQTESOLV (see Figures A-8 through A-10). It should be noted that in order to use AQTESOLV for the Theis recover method analysis, pumping of Wells 6 and 7 that occurred after the cessation of pumping in Well 5 could not be included in the analysis. Transmissivity determined from the recovery data for each well is somewhat higher than that determined using the Neuman-Witherspoon method. As indicated in Table A-3, the transmissivities determined using the Theis recovery method vary by a factor of approximately 2 to 13.

#### References

- Balaban, N.H. and H.C. Hobbs, 1990. Geologic Atlas Dakota County, Minnesota. Minnesota Geologic Survey, County Atlas Series, Atlas C-6.
- Duffield, G.M., 2000. AQTESOLV for Windows Ver.3.0. HydroSOLVE, Inc., Reston, Virginia.
- Kruseman, G.P. and N.A. de Ridder, 1991. <u>Analysis and Evaluation of Pumping Test Data</u>, 2<sup>nd</sup> edition, International Institute for Land Reclamation and Improvement, Wageningen, the Netherlands.
- Neuman, S.P. and P.A. Witherspoon, 1969. Applicability of Current Theories in Leaky Aquifers. Water Resources Research, Vol. 5, No. 4, p. 817-829.
- Theis, C.V., 1935. The Relation Between Lowering of the Piezometric Surface and the Rate and Duration of Discharge of a Well Using Groundwater Storage, Trans. Amer. Geophys. Union, Vol. 16, p. 519-524.
- Walton, W.C., 1987. <u>Groundwater Pumping Tests Design & Analysis</u>, Fifth Printing, Lewis Publishers, Inc., Chelsea, Michigan.

Table A-1
Well Construction Summary

Well Identification	Depth to Top of Jordan SS Aquifer (ft below ground surface)	Depth to Base of Jordan SS Aquifer (ft below ground surface)	Open Hole Interval (ft below ground surface)
Well 1(207821)	195	280	250-575
Well 3(206333)	197	>299	208-299
Well 4 (207993)	290	385	314-400
Well 5 (207639)	264	353	277-356
Well 6 (207643)	229	>332	240-332
Well 7(509053)	195	283	205-285

Well Identifi- cation	Unique Number	Easting (UTM NAD83)	Northing (UTM NAD83)	X Distance from Well 5 (m)	Y Distance from Well 5 (m)
Well 1*	207821	511658	4953826	2126	-109
Well 3	206333	510310	4954140	778	205
Well 4	207993	509649	4952285	117	-1650
Well 5	207639	509532	4953935	0	0
Well 6*	207643	512270	4951677	2738	-2258
Well 7*	509053	511352	4953764	1820	-171

<sup>\*</sup>Well not involved in the WHPA aquifer test.

Table A-2
Summary of Pumping Events During the Aquifer Testing Period

Time Since	Pumping Rates (gpm)					
Pumping Began in Well 5 (min.)	Well 5	Well 6	Well 7			
0	1089	0	554.7			
315	805	0	544.7			
500	818	0	554.7			
1170	818	0	0			
1290	813	0	0			
1365	813	1003.8	0			
1440	0	1003.8	1209.7			
1533	0	0	1209.7			
1598	0	0	0			
1695	0	1003.8	0			
1768	0	1003.8	1209.7			
1826	0	1003.8	0			
1893	0	0	0			
1946	0	0	1209.7			
2021	0	0	0			
2055	0	1003.8	0			
2141	0	0	1209.7			
2216	0	0	0			
2253	0	0	0			
2351	0	0	1209.7			
2415	0	1003.8	1209.7			
2426	0	1003.8	0			
2651	0	0	1209.7			
2741	0	0	0			

Table A-3
Aquifer Test Results Summary

			itherspoon	Theis-Recovery		
		Transmissivity		Transmissivity		
Well#	Test Phase	(m²/day)	Storage Coefficient	(m²/day)	Storage Coefficient	
Well 3	Pumping & Recovery	324.0	8.05 <sup>-5</sup>	na	na	
	Recovery only	na	na	651.4	S'=2.296	
Well 4	Pumping & Recovery	143.9	3.33x10 <sup>-5</sup>	na	na	
	Recovery only	na	na	1912.4	S'=2.5	
Well 5	Pumping & Recovery	355.0	1.21x10 <sup>-4</sup>	na		
	Recovery only	na	na	812.2	S'=3.162	

Geometric Mean				
Transmissivity				
(m²/day)	Storage Coefficient			
505.8	6.87x10 <sup>-5</sup>			

Note: Geometric mean of the transmissivity calculated using results from both the Neuman-Witherspoon and Theis-recovery analyses. Geometric mean of the storage coefficient calculated using results of only the Neuman-Witherspoon analyses.

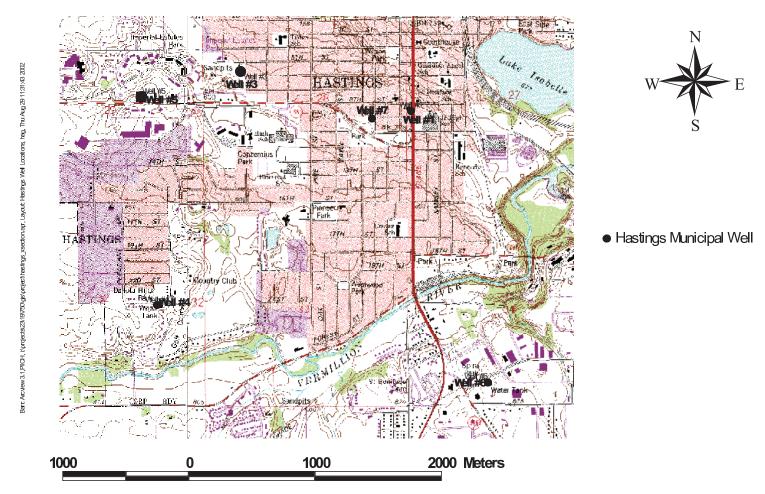


Figure A-1 Hastings Municipal Well Locations

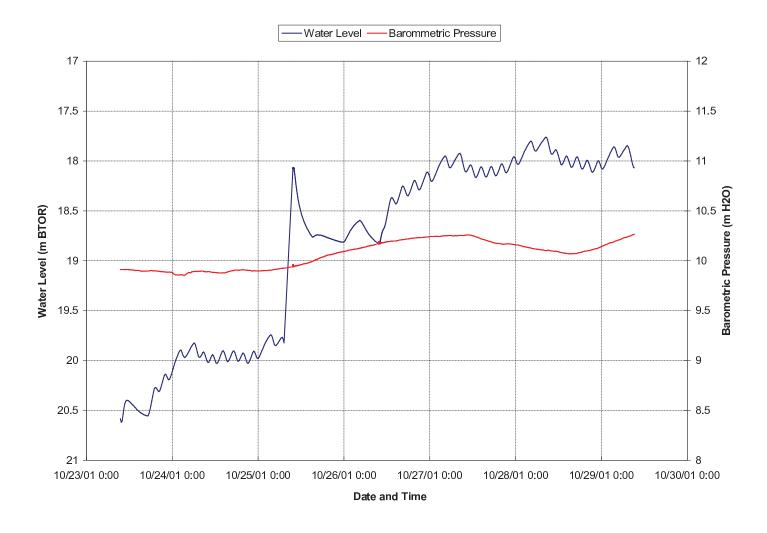


Figure A-2
Hydrograph for Hastings Well 3

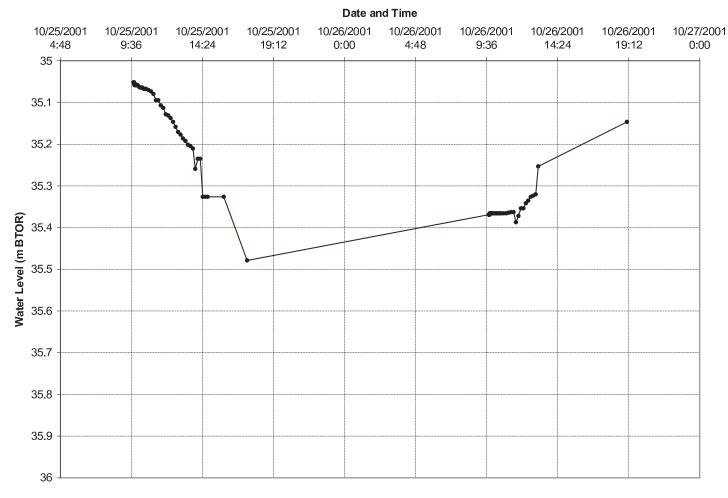


Figure A-3
Hydrograph for Hastings Well 4

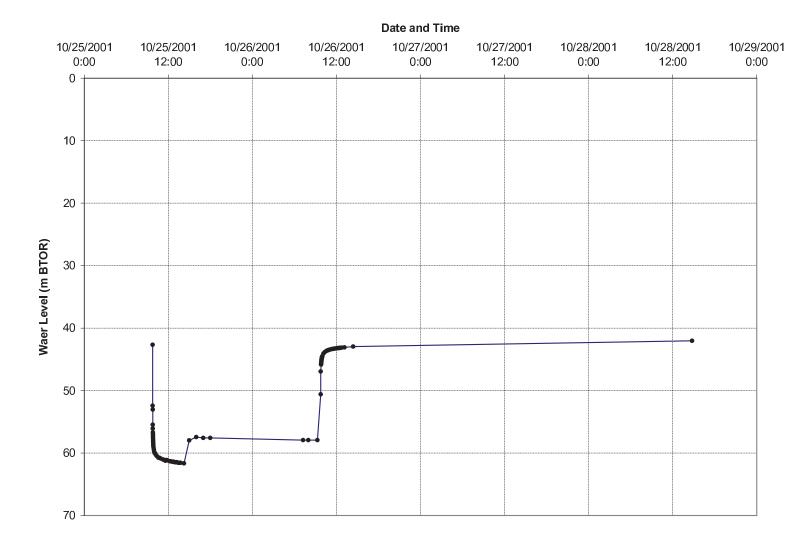


Figure A-4
Hydrograph for Hastings Well 5

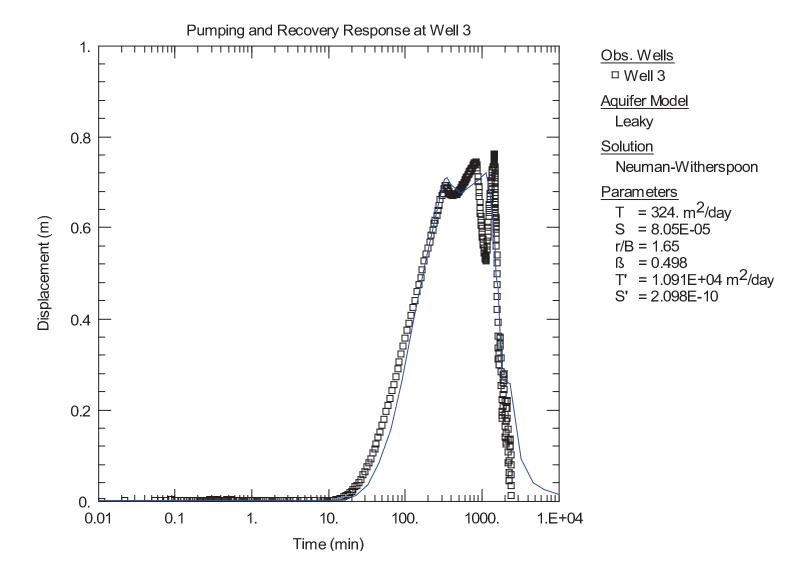


Figure A-5
Analysis of Well 3 Drawdown and Recovery Data

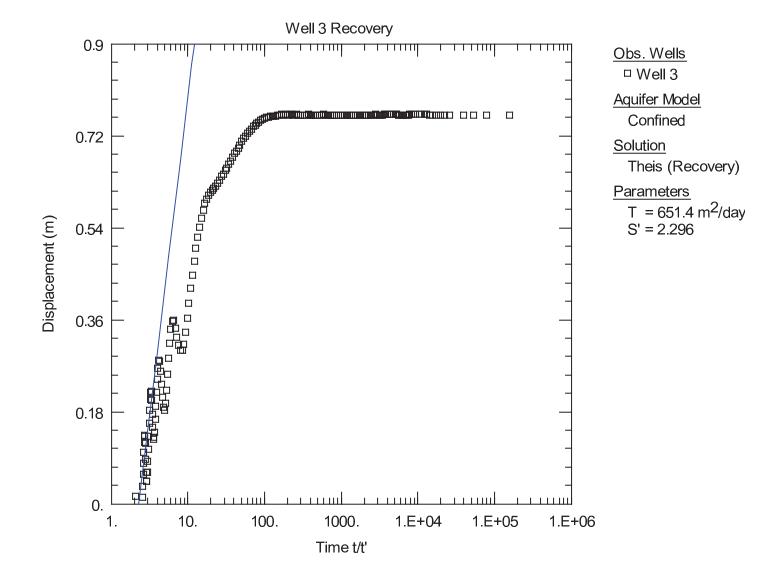


Figure A-8
Analysis of Well 3 Recovery Data

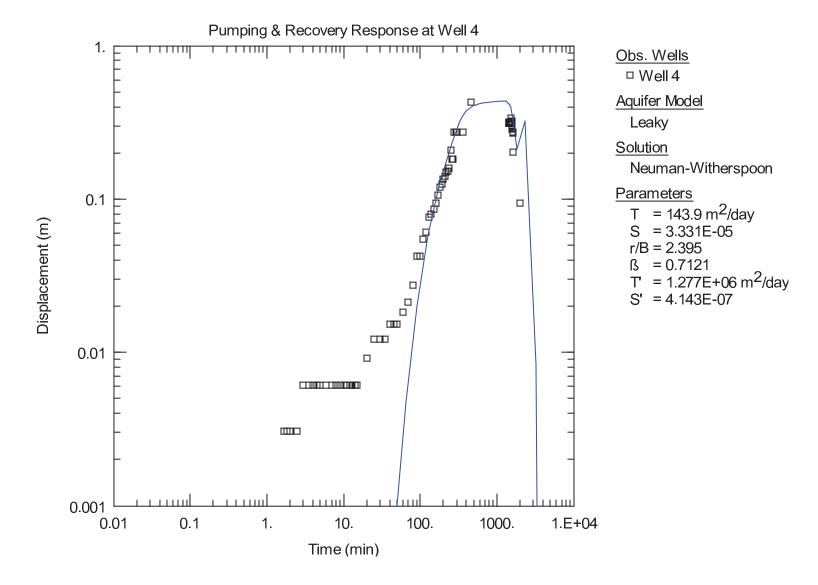


Figure A-6
Analysis of Well 4 Drawdown and Recovery Data

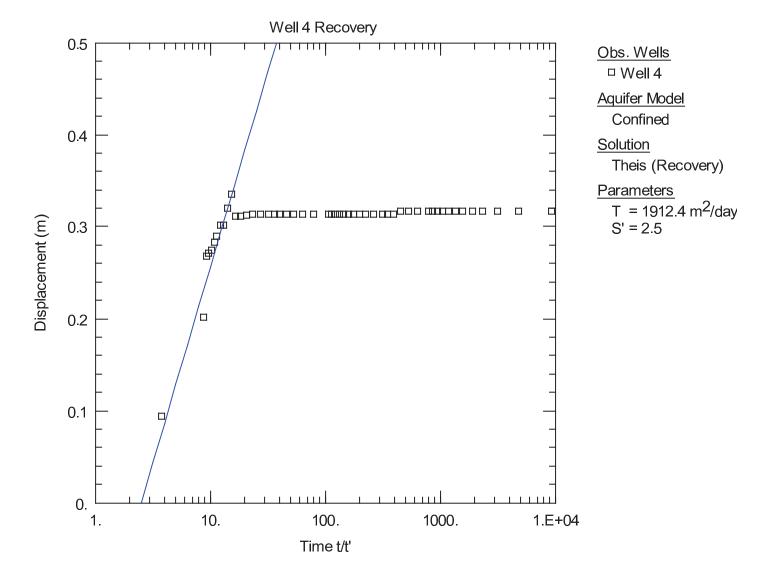


Figure A-9
Analysis of Well 4 Recovery Data

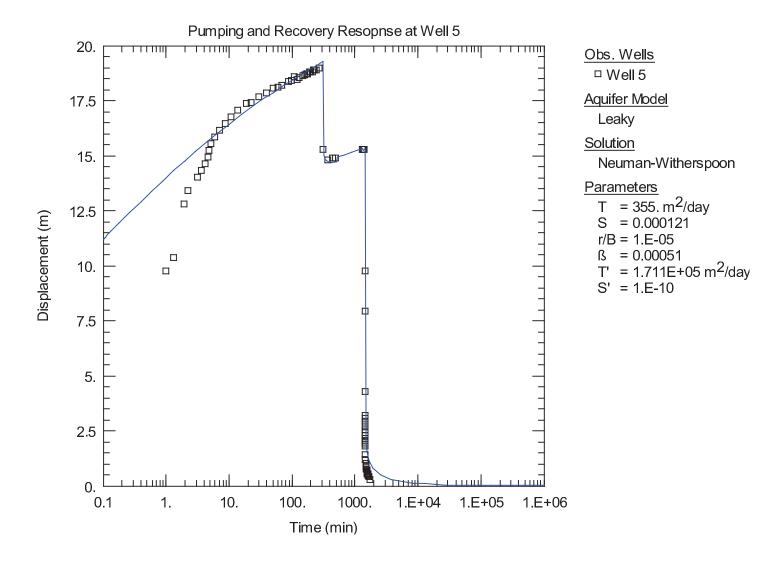
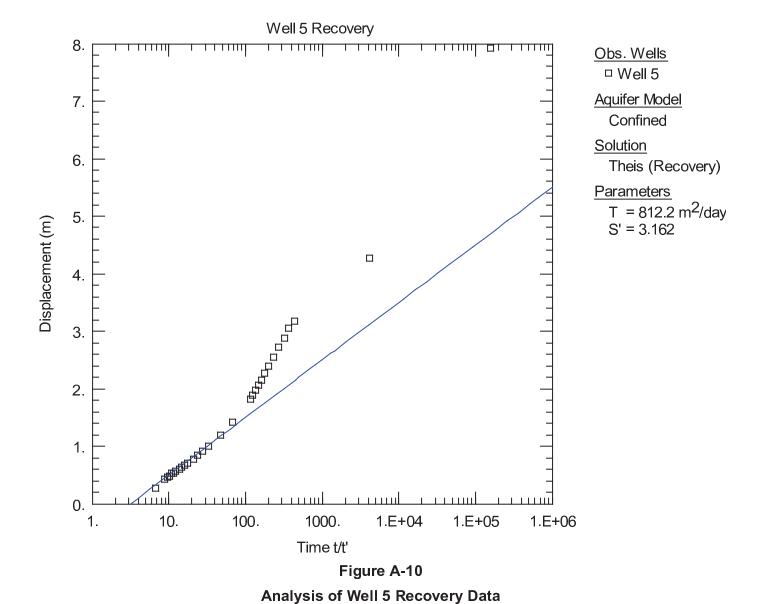


Figure A-7
Analysis of Well 5 Drawdown and Recovery Data

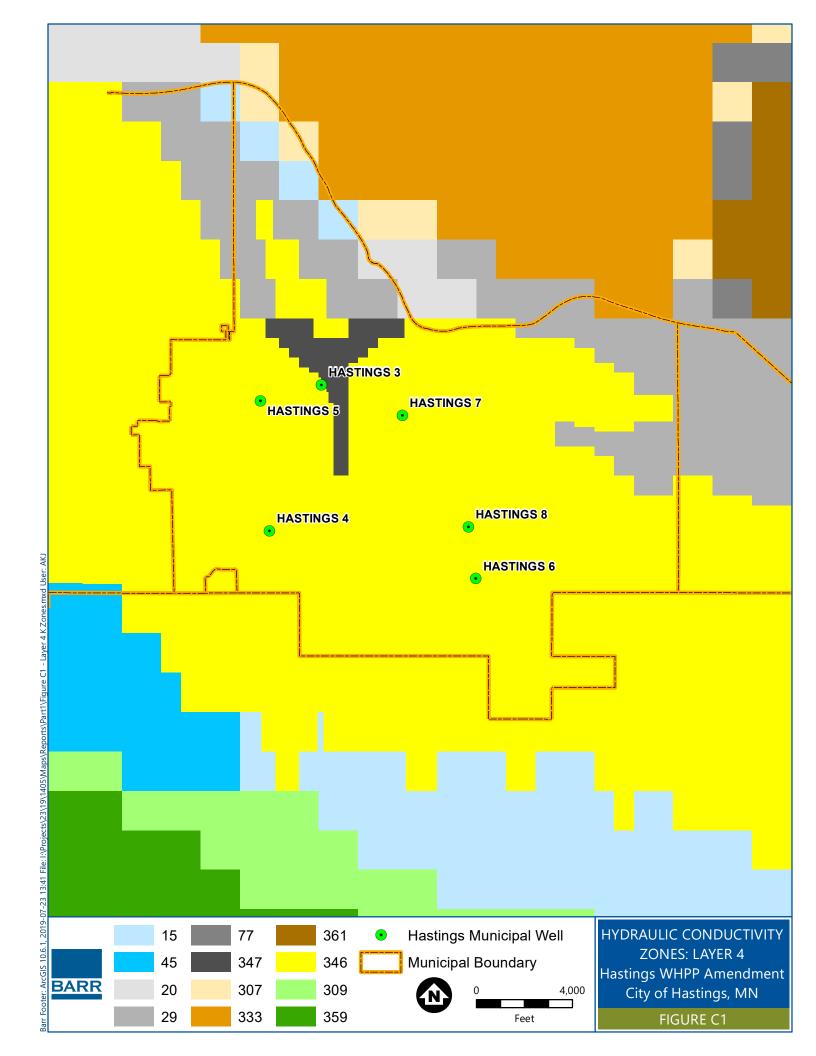


### Appendix C

**Groundwater Model Details** 

Table C1
Updated High-Capacity Pumping
Hastings WHPP Amendment

Unique				Annual Pump	ed Volume (m	nillion gallons	)	2013-2017	Average
Number	Name	Permit	2017	2016	2015	2014	2013	gpm	m³/d
250177	Bauer, Loren; Bauer, Willard	1969-1102	17.8000	8.2250	30.8360	33.7730	46.9840	52.34	285.31
121821	Bauer, Robert	1975-6126	18.3600	17.2800	18.9600	45.4400	61.9000	61.59	335.74
251398	Ardent Mills	1975-6278	6.8335	8.8863	11.4520	7.7116	6.6392	15.79	86.08
170868	Finnegan, David	1975-6358	22.4000	23.1500	23.2000	23.6248	23.6250	44.12	240.49
236554	Bauer, Jerry	1975-6374	18.4440	15.3180	24.7470	27.6960	41.5170	48.57	264.79
(blank)	Bauer, Loren	1976-6084	15.2800	11.3000	26.1500	34.6500	46.3600	50.86	277.27
250020	Becker, Edward	1976-6157	21.6672	14.8464	16.0515	24.8355	34.9440	42.73	232.91
121847	Bauer, Brian	1976-6184	11.9586	11.5347	15.4500	19.6052	29.2862	33.40	182.10
257402	Ries, Marcelline; Ries, Nick	1976-6204	49.0650	36.0000	17.6723	20.8517	41.1832	62.66	341.61
216367	Bauer, Loren	1977-6441	16.9500	11.7500	23.5300	39.5600	39.7220	50.02	272.65
255924	Ind School District 200	1978-6167	0.3360	0.0721	0.7550	0.5107	0.8807	0.97	5.30
242343	Bauer, Loren	1978-6190	14.4920	12.5000	28.2960	32.8520	37.6200	47.83	260.73
207642	Mn Dept Of Veterans Affairs	1985-6224	0.0250	0.0000	0.3350	0.4050	0.5590	0.50	2.74
749829	Mn Dept Of Veterans Affairs	1985-6224	0.0000	0.0000	0.0000	0.0960	0.0960	0.07	0.40
771760	Mn Dept Of Veterans Affairs	1985-6224	7.8400	7.1600	6.4370	8.0060	7.6000	14.09	76.80
207640	All Pro Holdings, LLC d.b.a. Dakota Pines Golf Club	1986-6243	18.1799	15.2725	15.6998	13.4913	30.8863	35.57	193.91
672739	All Pro Holdings, LLC d.b.a. Dakota Pines Golf Club	1986-6243	12.4003	10.1817	10.4532	8.9942	0.0000	15.98	87.14
(blank)	Barton Sand and Gravel Co.	1993-6152	0.0600	0.0552	0.0650	0.0650	0.0000	0.09	0.51
603062	Ind School District 200	2005-3014	0.5450	0.2381	0.7366	1.7752	2.2725	2.12	11.54
672578	Ind School District 200	2005-3014	0.1432	0.0684	0.3920	0.5838	0.7687	0.74	4.06
121088	Pettit, Marlene	2006-0420	3.1620	2.8050	3.0600	6.5790	5.8140	8.15	44.41
768670	Wagner, Ralph	2015-1357	6.3580	4.9800	12.0037	12.0037		16.80	91.59
806056	Mulvihill, Glenn M	2015-1392	11.9102	8.9401	7.4996			17.96	97.92



## Figure C2 Model Calibration Hastings WHPP Amendment

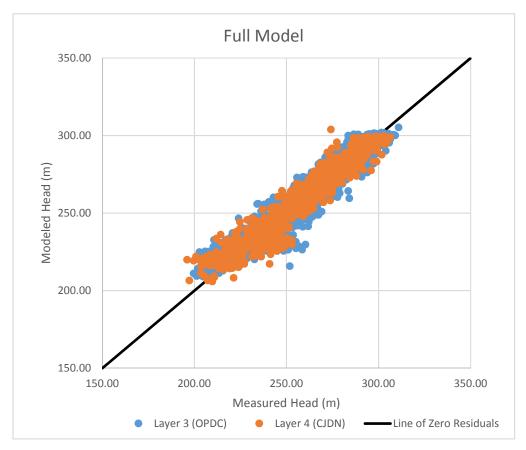
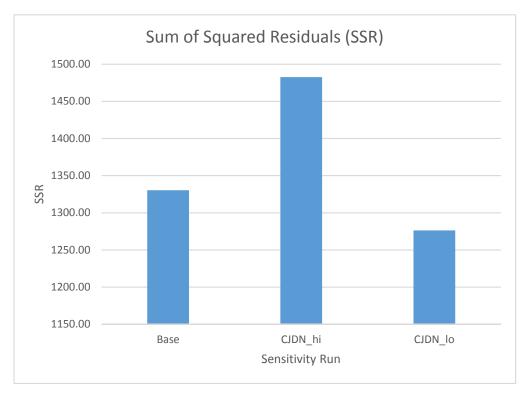
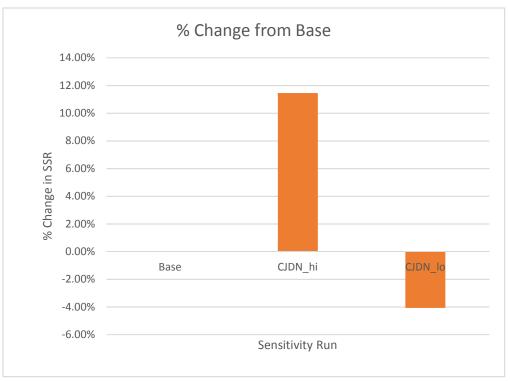




Figure C3
Sensitivity Analysis Summary
Hastings WHPP Amendment





Note: Results shown for Layer 4 targets within 2 miles of Hastings only

### Appendix D

**Fracture Flow Delineation** 

## Table D1 Estimated Contributions from Prairie du Chien Group Hastings WHPP Amendment

		Well Pumping	Base Model Net Layer 3 Contribution to Layer 4 Capture Zone (m <sup>3</sup> /day)			
Unique	Well	Rate (m³/day)	(m³/day)	% of pumping rate		
206333	3	1,438	1,098	76%		
207993	4	1,947	829	43%		
207639	5	1,508	296	20%		
207643	6	1,441	311	22%		
509053	7	2,483	1,788	72%		
686266	8	1,535	720	47%		

## Table D2 Fracture Flow Tool Input Hastings WHPP Amendment

Unique	Well	Model Pumping Rate (m³/day)	Fraction from OPDC	Fracture Flow Pumping Rate (m³/day)	OPDC Thickness from Log <sup>1</sup> (ft)	OPDC Thickness to Use (ft)		Gradient	Q/Qs (m)	Upgradient Extension Required?	Bearing (degrees east of north)
206333	3	1,438	0.76	1098	268	200	33.45	0.0022	249	YES	234
207993	4	1,947	0.43	829	234	200	33.45	0.0022	188	YES	221
207639	5	1,508	0.20	296	268	200	33.45	0.0022	67	YES	235
207643	6	1,441	0.22	311	136	136	33.45	0.0022	104	YES	220
509053	7	2,483	0.72	1788	136	136	33.45	0.0022	597	YES	225
686266	8	1,535	0.47	720	181	181	33.45	0.0022	181	YES	217

<sup>&</sup>lt;sup>1</sup> Actual OPDC thickness at Well 3 is zero, assumed thickness from nearby Well 5 for fracture flow calcs

$$Q/Qs = \frac{Q\left(\frac{1ft^3}{7.48gal}\right)\left(\frac{1440\min}{1day}\right)\left(\frac{0.0283m^3}{1ft^3}\right)}{(H)\left(\frac{0.3048m}{1ft}\right)(K)(i)}$$

## Table D3 Overlapping High Capacity Wells Hastings WHPP Amendment

	OPDC Thickness from Log <sup>1,2,3</sup>	OPDC Thickr	ness to Use	Model Pumping Rate	10-year Fixed Radius	Overlaps with	Overlapping Area
Unique	(ft)	(ft)	(m)	(m³/day)	(m)	Hastings well	(m²)
121847	19	19	5.79	182.10	807.70	none	0
207640	235	200	60.96	193.91	256.89	4	97625.18
207642	137	137	41.76	2.74	36.90	none	0
250177	234	200	60.96	285.31	311.61	none	0
251398	187	187	57.00	86.08	177.01	8	62380.58
255924	136	136	41.45	5.30	51.50	7	8311.23
408251	191	191	58.22	176.54	250.83	none	0
672739	185	185	56.39	87.14	179.06	none	0
771760	149	149	45.42	76.80	187.31	8	2791.52
806056	19	19	5.79	97.92	592.28	none	0

<sup>&</sup>lt;sup>1</sup> No OPDC thickness on log for well 250177. Used thickness from Hastings 4.

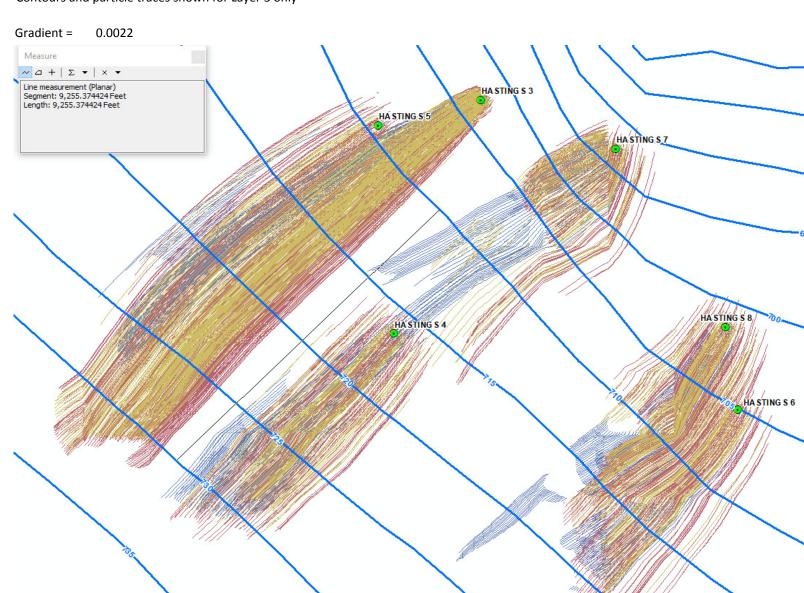
Porosity 0.056

Unique	Well	Preliminary 5-year Fixed Radius Capture Zone Area (m²)	Total Overlapping Area (m²)	Adjusted Area (m²)	Adjusted 5- year Fixed Radius (m)	Effective Pumping Rate for Fracture Flow Tool (m³/day)
206333	3	586813.36	0	586813.3573	432.19	1098
207993	4	443029.01	97625.18	540654.1972	414.84	1011
207639	5	158149.29	0	158149.2943	224.37	296
207643	6	244385.89	0	244385.8913	278.91	311
509053	7	1405407.37	8311.23	1413718.6	670.82	1798
686266	8	425164.52	65172.10	490336.6127	395.07	830

<sup>&</sup>lt;sup>2</sup> No OPDC thickness on log for well 255924. Used thickness from Hastings 7.

 $<sup>^{3}</sup>$  No log for well 806056. Used thickness from well 121847.

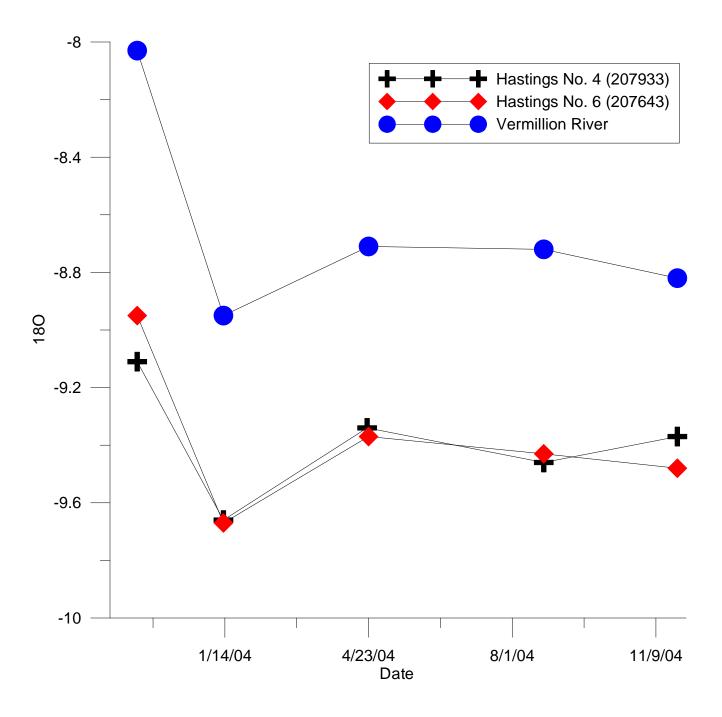
#### Contours and particle traces shown for Layer 3 only



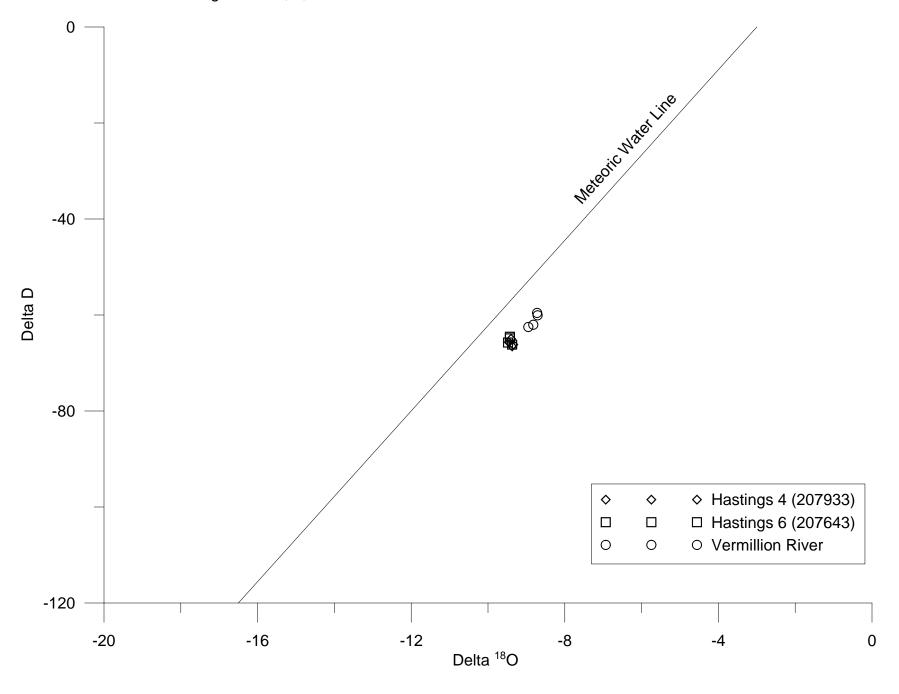
Appendix E

Isotope Data

Figure 1. Oxygen Isotope Results Show Close Correlation Between Vermillion River and Hastings Wells

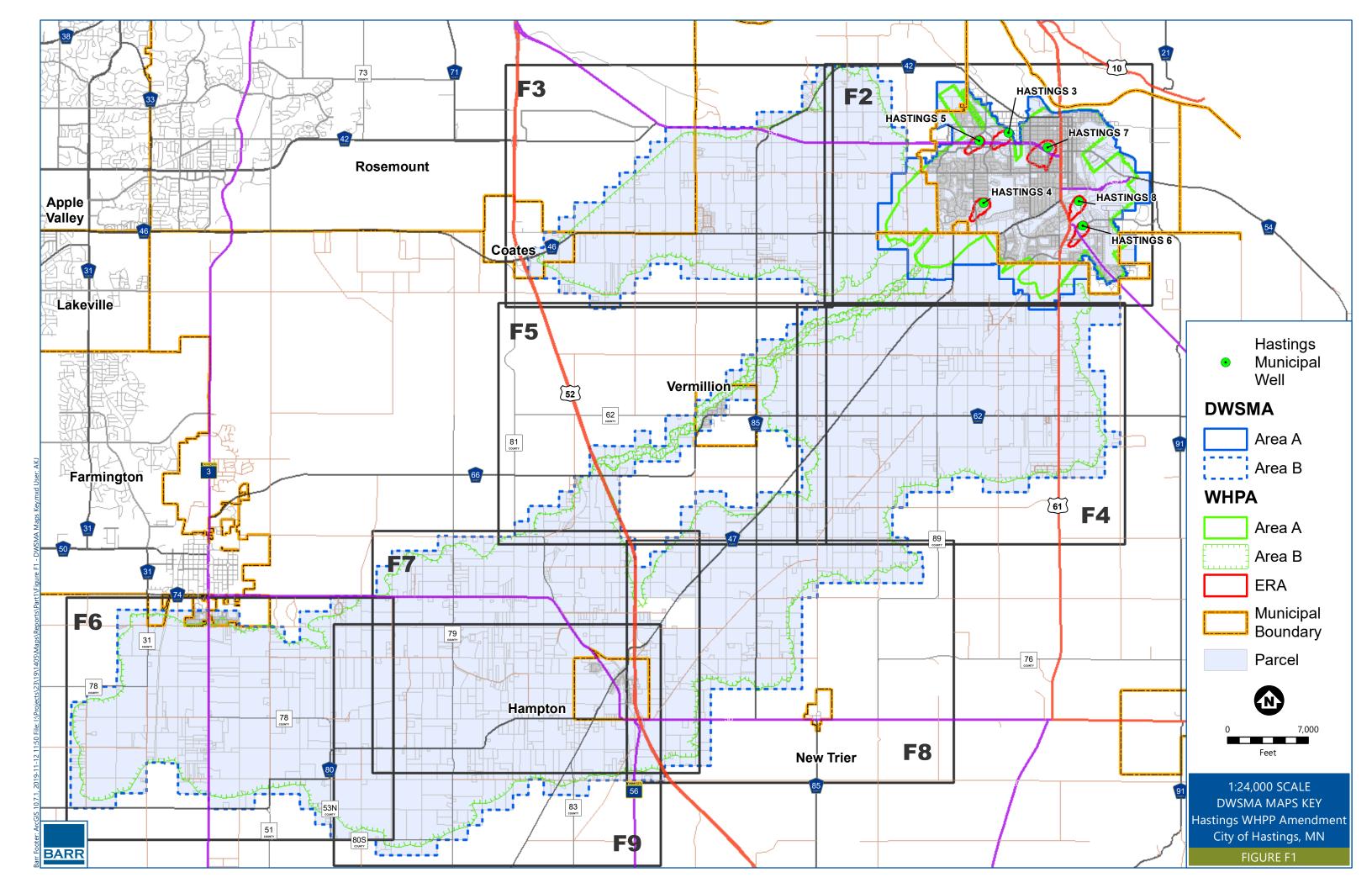


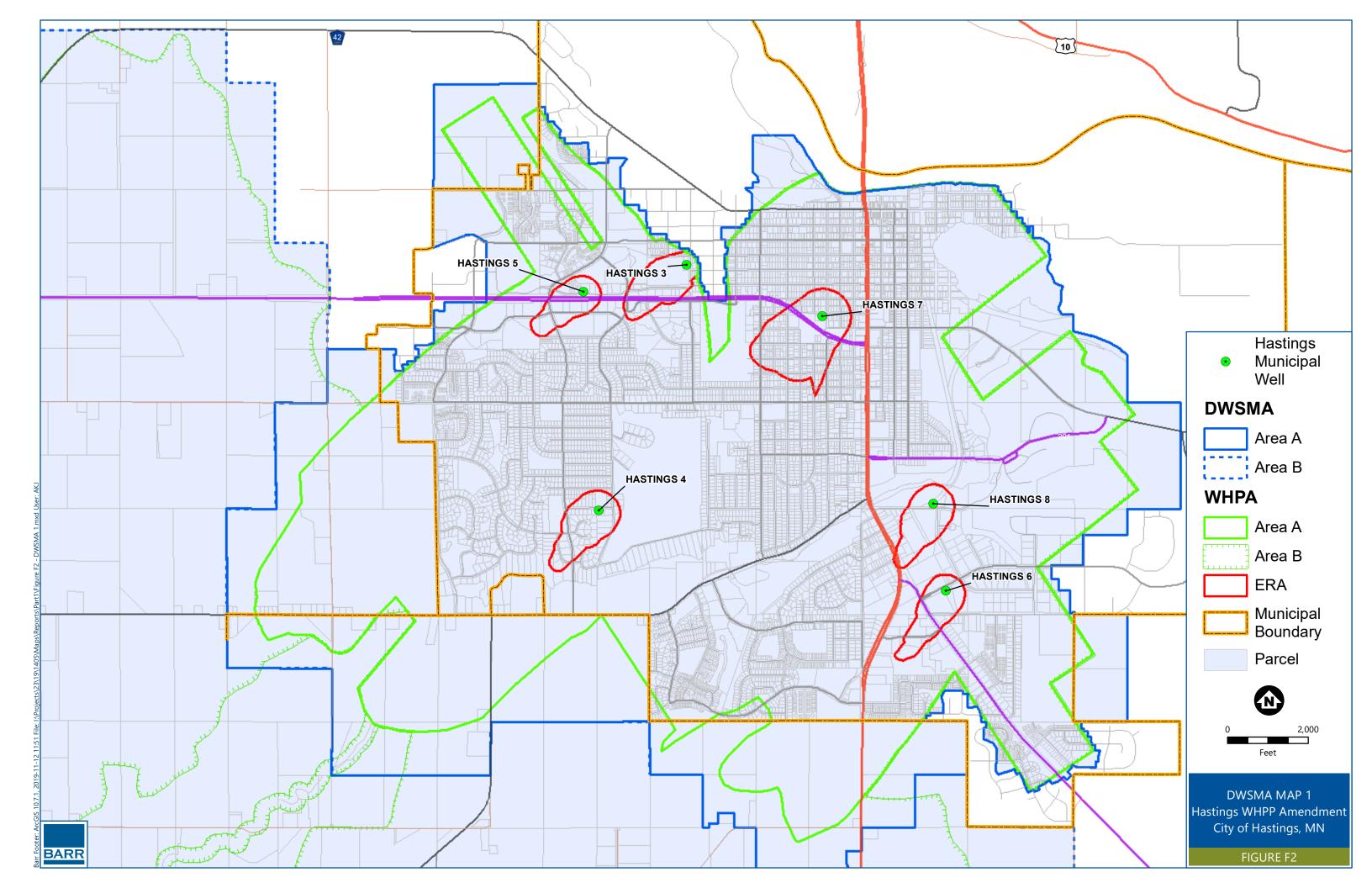
Oxygen and Hydrogen Isotope Analysis Hastings Wells 4, 6, and Vermillion River

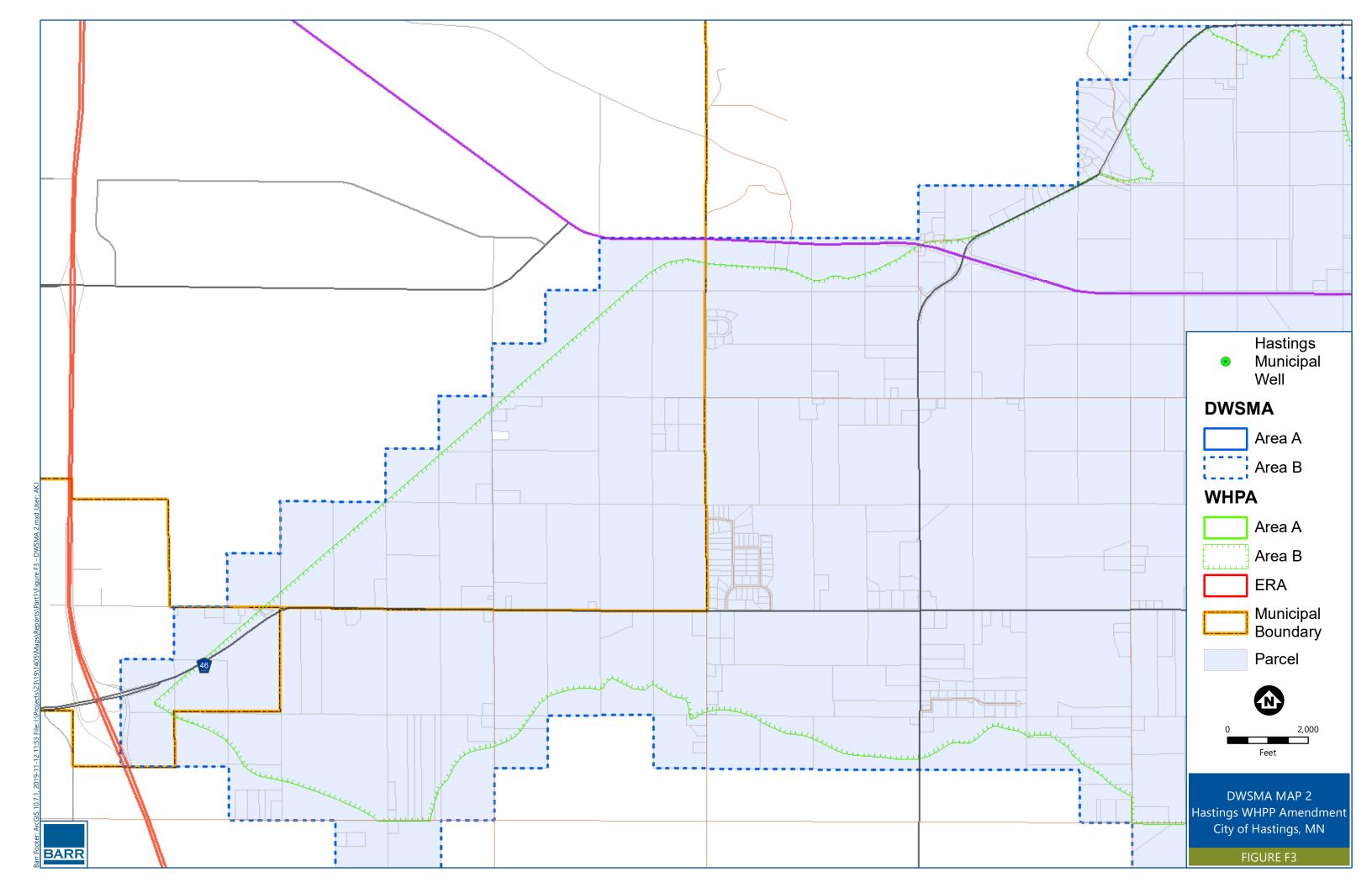


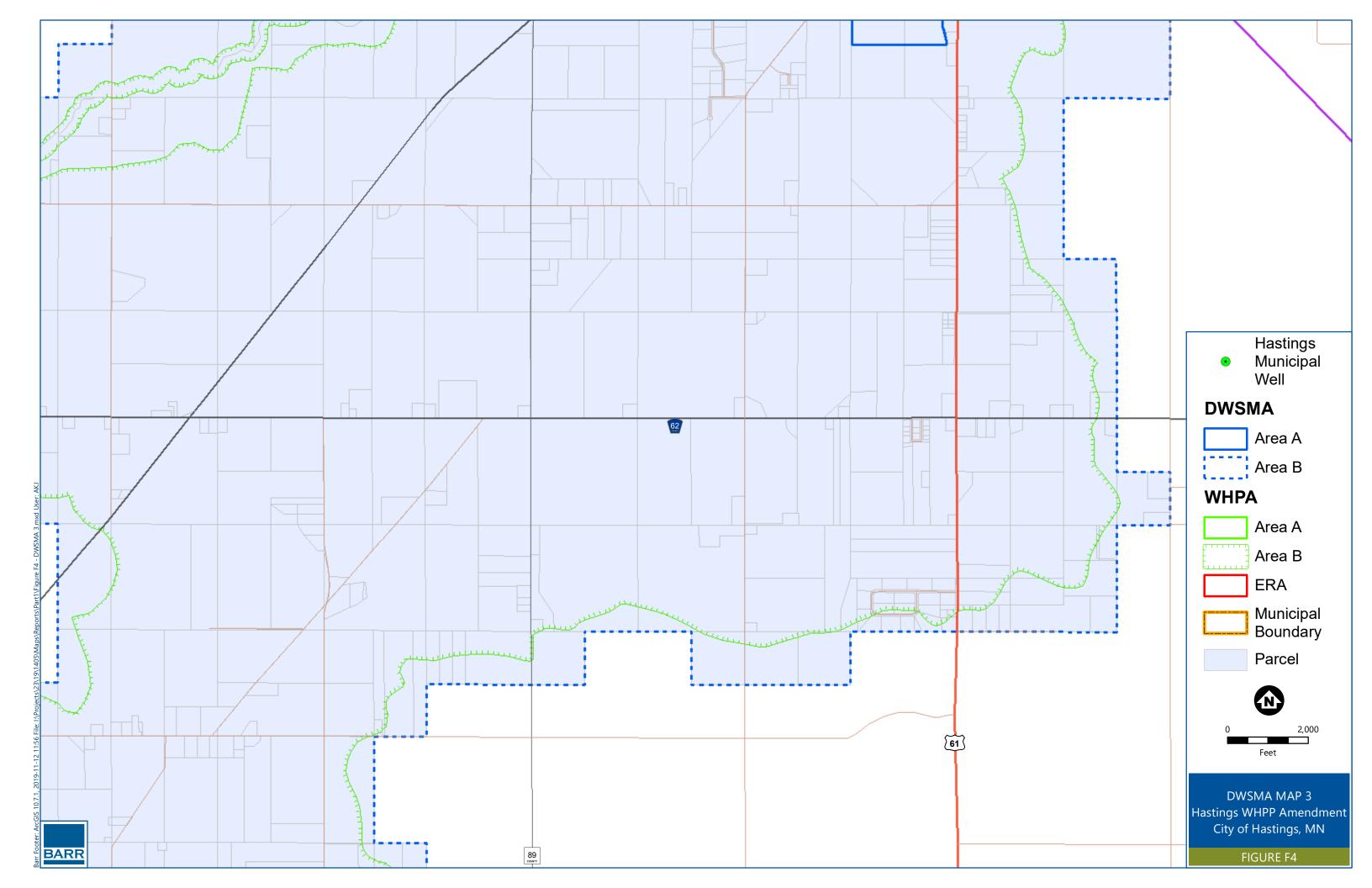
### Appendix F

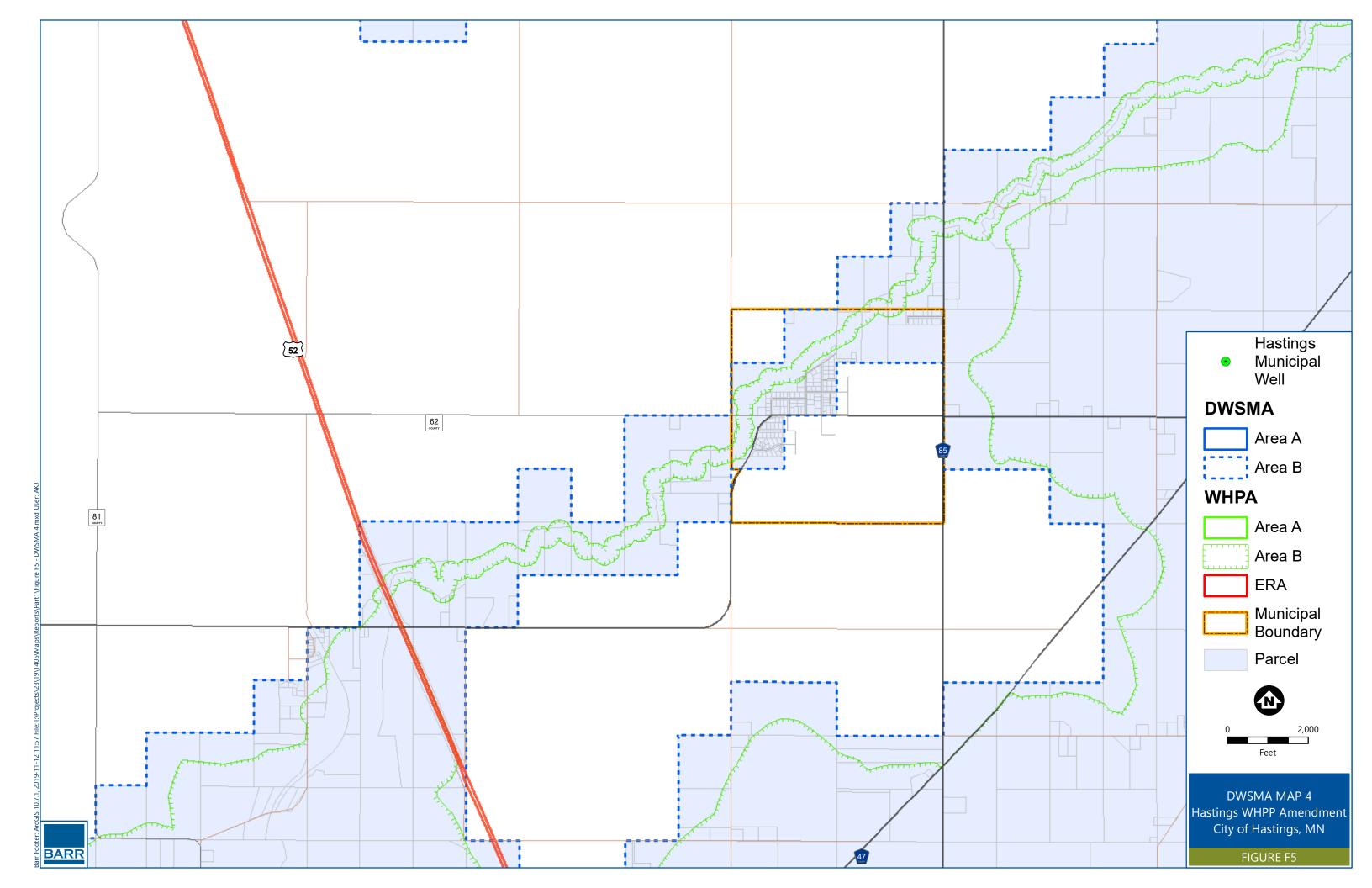
1:24,000 Scale DWSMA Maps

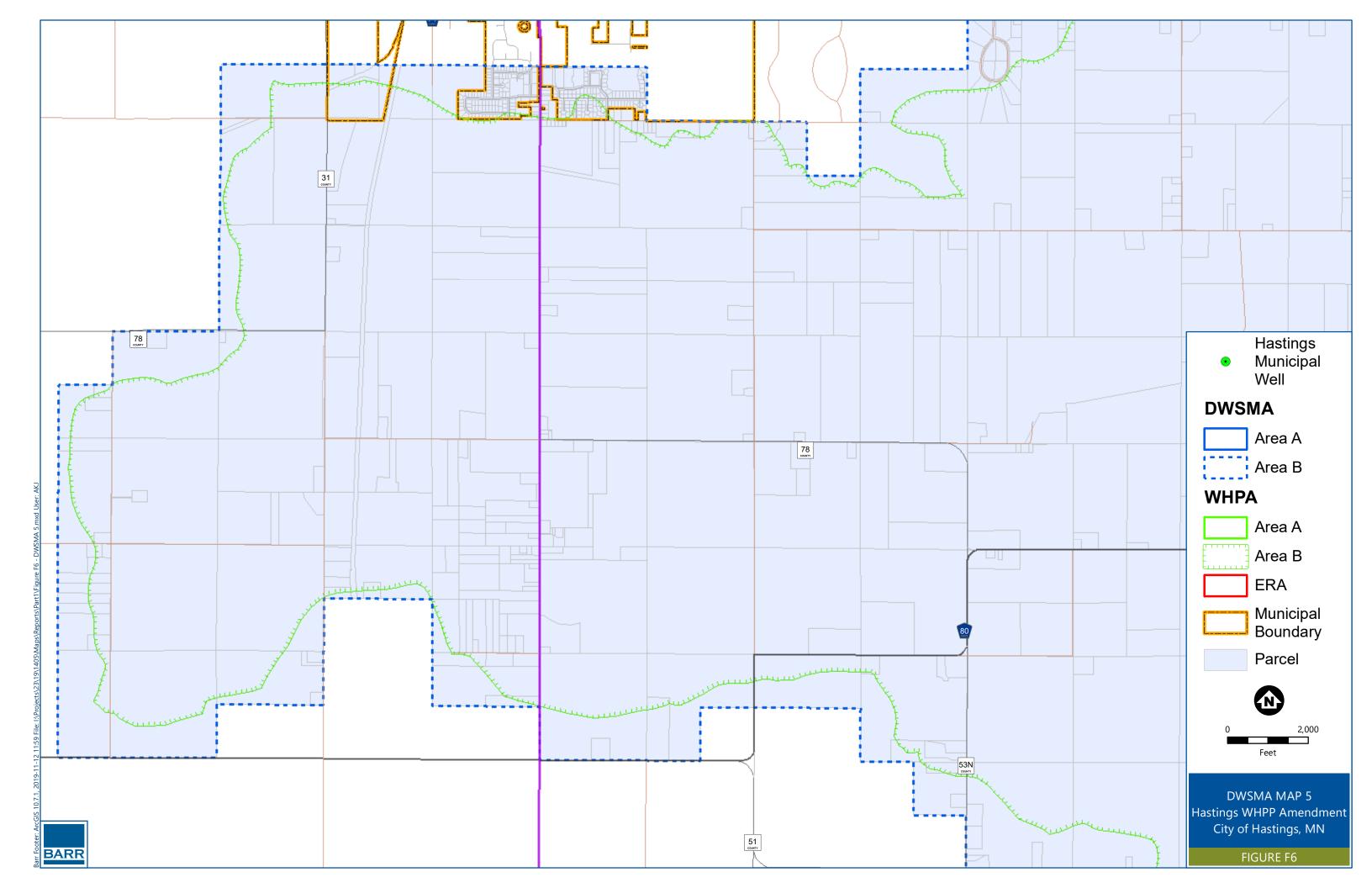


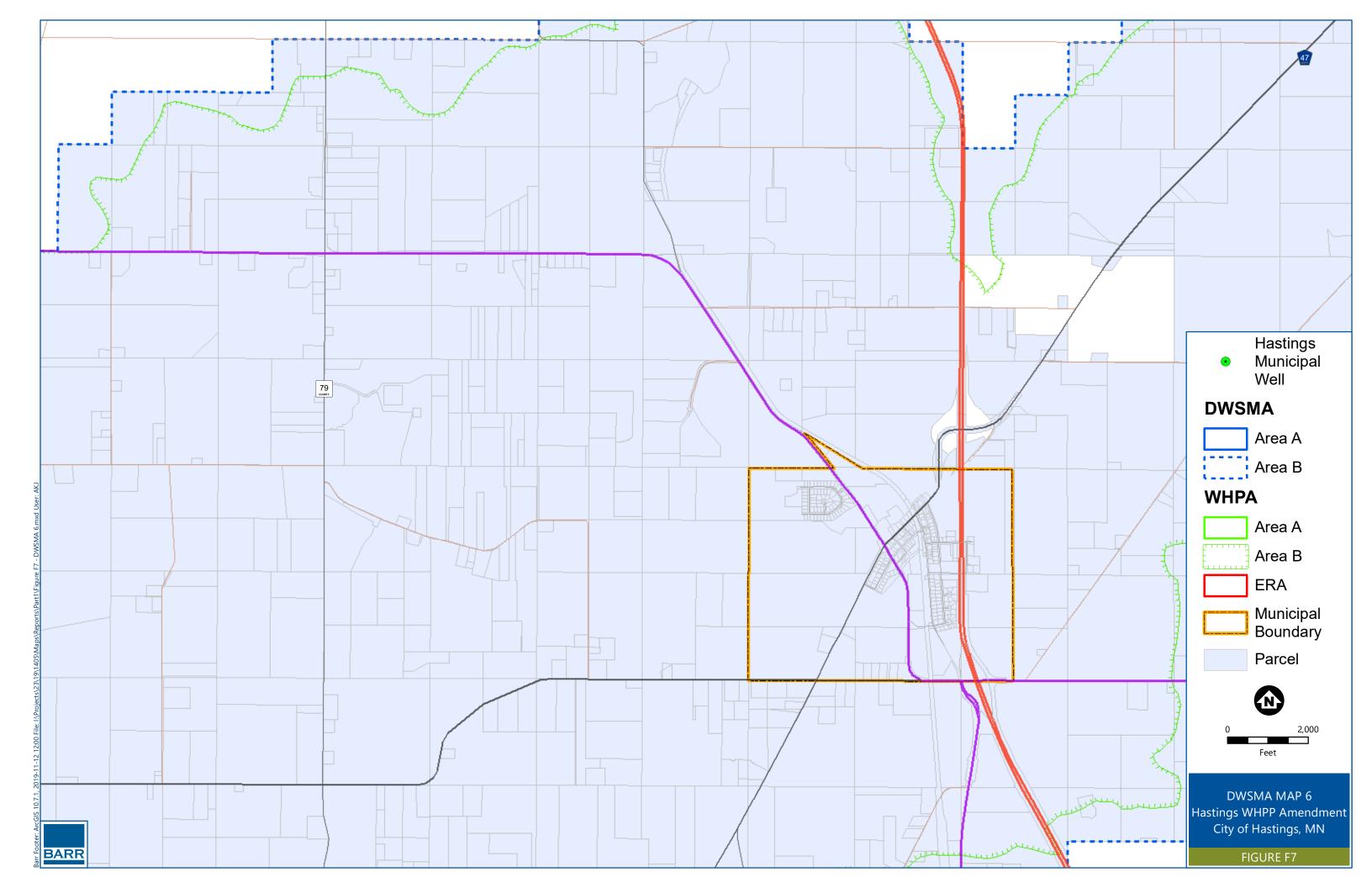


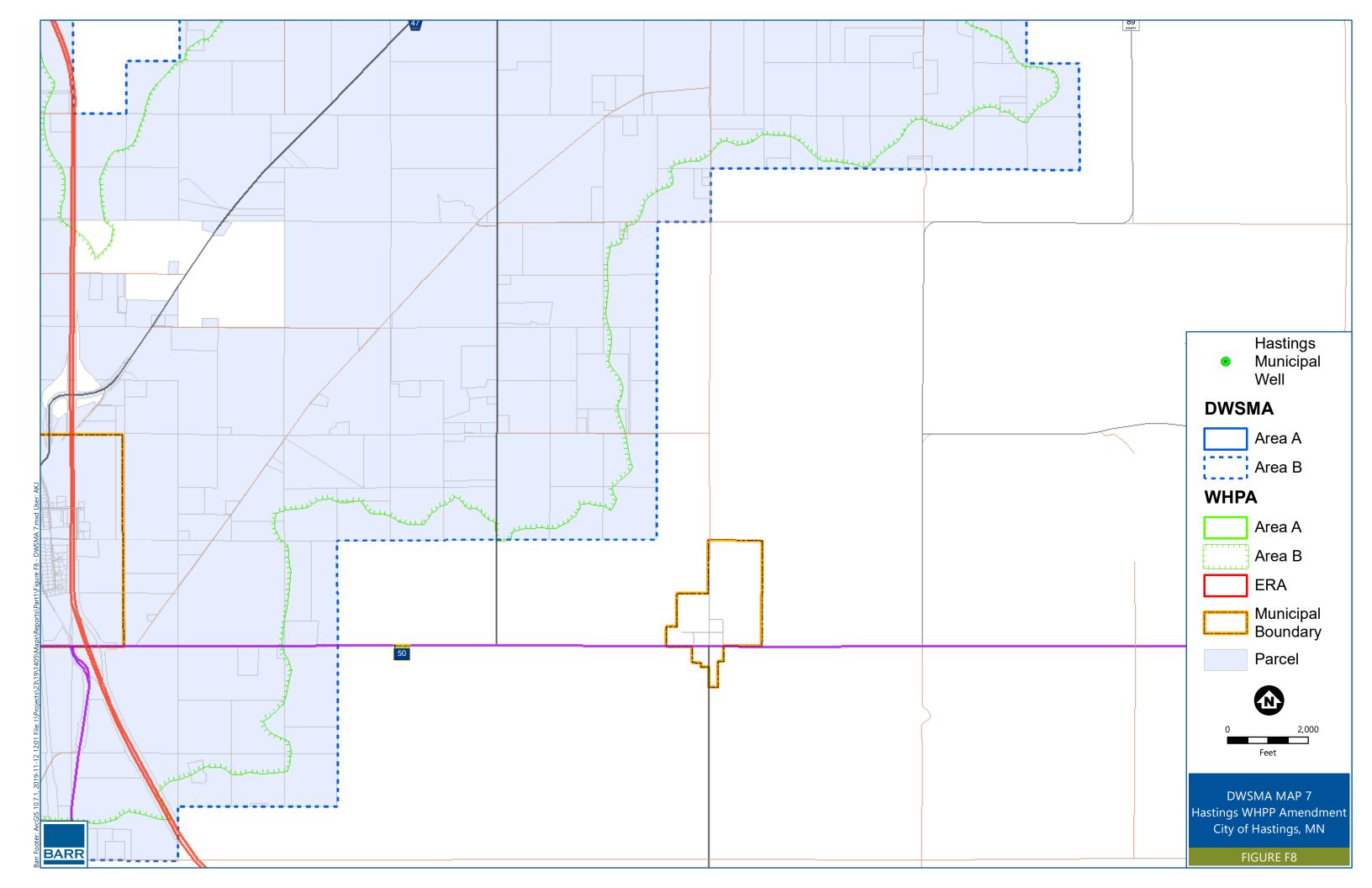


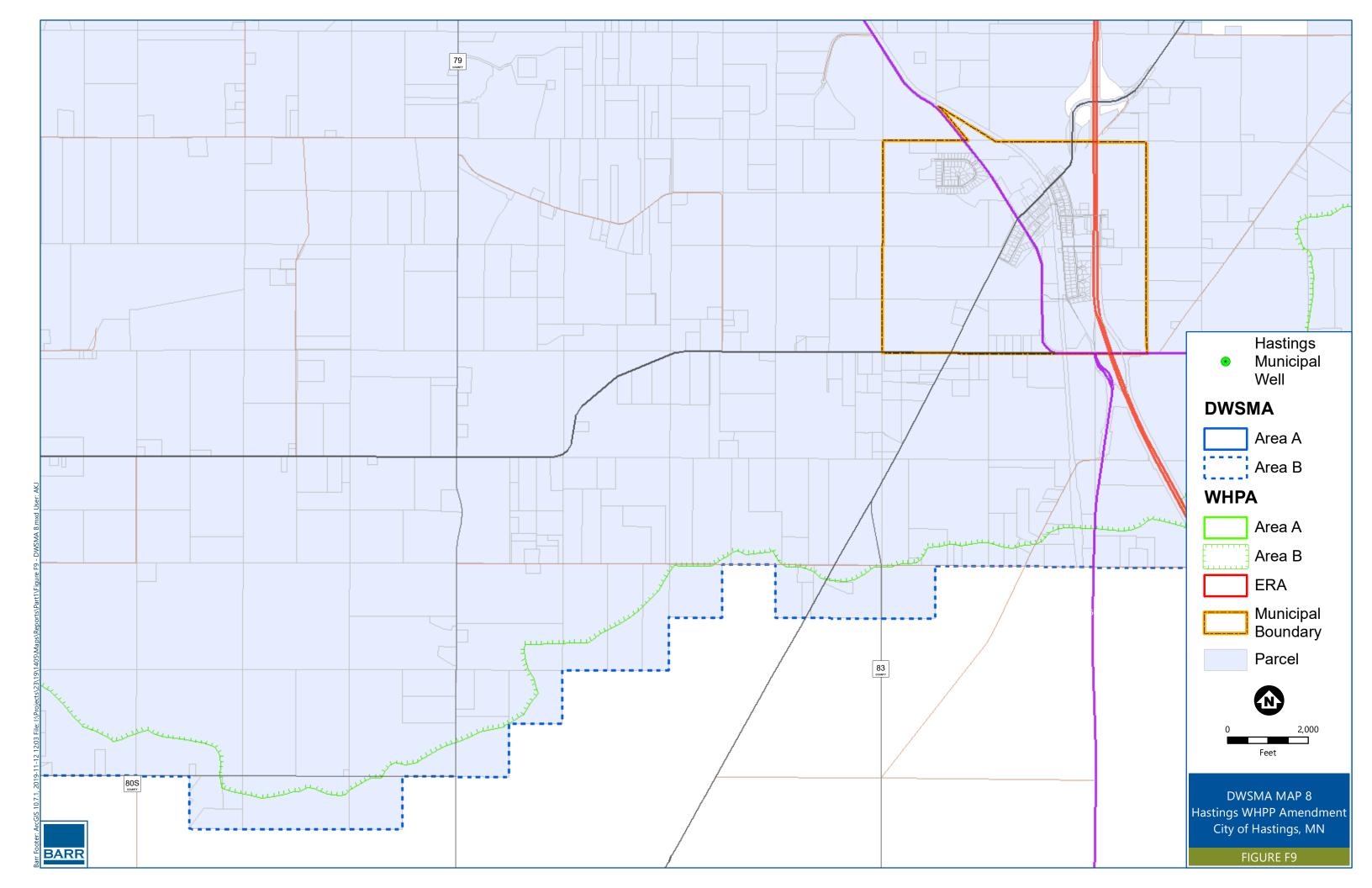












### Appendix G

**MDH Well Vulnerability Assessments** 





625 Robert St. N. St. Paul MN 55155 P.O. Box 64975 St. Paul MN 55164 - 0975

PWSID: 1190012 TIER: 1
SYSTEM NAME: Hastings WHP RANK:

WELL NAME: Well #3 UNIQUE WELL #: 00206333

COUNTY: Dakota	TOWNSHIP	NUMBER: 115 RANGE:	17 W SE	ECTION: 28 QUAF	RTERS: BCAC
<u>CRITERIA</u>		DESCRIPTION		POII	<u>NTS</u>
Aquifer Name(s)	:	Jordan			
DNR Geologic Sensitivity Rating	:	Very low		10	
L Score	:	9			
Geologic Data From	:	Well Record			
Year Constructed	:	1956			
Construction Method	:	Cable Tool/Bored		0	
Casing Depth	:	208		5	
Well Depth	:	299			
Casing grouted into borehole?		Yes		0	
Cement grout between casings?		Yes		0	
All casings extend to land surface?		Yes		0	
Gravel - packed casings?		No		0	
Wood or masonry casing?		No		0	
Holes or cracks in casing?		Unknown		0	
Isolation distance violations?				0	
Pumping Rate	:	1000		10	
Pathogen Detected?				0	
Surface Water Characteristics?				0	
Maximum nitrate detected	:	9 04/29/2004		30	
Maximum tritium detected	:	Unknown		0	
Non-THMS VOCs detected?		Trichloroethene (TCE)	09/14/19	90 VUL	NERABLE
Pesticides detected?		Atrazine	08/15/198	39 VUL	NERABLE
Carbon 14 age	:	Unknown		0	
Wellhead Protection Score	:			55	
Wellhead Protection Vulnerability Rat	ing:			VUL	NERABLE

Vulnerability Overridden :





625 Robert St. N. St. Paul MN 55155 P.O. Box 64975 St. Paul MN 55164 - 0975

PWSID: 1190012 TIER: 1
SYSTEM NAME: Hastings WHP RANK:

WELL NAME: Well #4 UNIQUE WELL #: 00207993

COUNTY: Dakota	TOWNSH	IP NUMBER: 115 RANGE: 17 W	SECTION: 32 QUARTERS: DABB
CRITERIA		DESCRIPTION	<u>POINTS</u>
Aquifer Name(s)	:	Jordan	
DNR Geologic Sensitivity Rating	:	Low	20
L Score	:	2	
Geologic Data From	:	Well Record	
Year Constructed	:	1961	
Construction Method	:	Cable Tool/Bored	0
Casing Depth	:	314	5
Well Depth	:	400	
Casing grouted into borehole?		Yes	0
Cement grout between casings?		Yes	0
All casings extend to land surface?		Yes	0
Gravel - packed casings?		No	0
Wood or masonry casing?		No	0
Holes or cracks in casing?		Unknown	0
Isolation distance violations?			0
Pumping Rate	:	1000	10
Pathogen Detected?			0
Surface Water Characteristics?			0
Maximum nitrate detected	:	4.1 09/12/2016	30
Maximum tritium detected	:	3.7 03/29/2016	VULNERABLE
Non-THMS VOCs detected?			0
Pesticides detected?			0
Carbon 14 age	:	Unknown	0
Wellhead Protection Score	:		65
Wellhead Protection Vulnerability Rat	ing :		VULNERABLE

Vulnerability Overridden :





625 Robert St. N. St. Paul MN 55155 P.O. Box 64975 St. Paul MN 55164 - 0975

PWSID: 1190012 TIER: 1
SYSTEM NAME: Hastings WHP RANK:

WELL NAME: Well #5 UNIQUE WELL #: 00207639

COUNTY: Dakota	TOWNSH	P NUMBER: 115 RANGE: 17 W	SECTION: 29 QUARTERS: ACDD
CRITERIA		DESCRIPTION	<u>POINTS</u>
Aquifer Name(s)	:	Jordan	
DNR Geologic Sensitivity Rating	:	High	VULNERABLE
L Score	:	0	
Geologic Data From	:	Well Record	
Year Constructed	:	1970	
Construction Method	:	Cable Tool/Bored	0
Casing Depth	:	277	5
Well Depth	:	355	
Casing grouted into borehole?		Unknown	0
Cement grout between casings?		Yes	0
All casings extend to land surface?		Yes	0
Gravel - packed casings?		No	0
Wood or masonry casing?		No	0
Holes or cracks in casing?		Unknown	0
Isolation distance violations?			0
Pumping Rate	:	1225	20
Pathogen Detected?			0
Surface Water Characteristics?			0
Maximum nitrate detected	:	8.7 06/03/2008	30
Maximum tritium detected	:	Unknown	0
Non-THMS VOCs detected?			0
Pesticides detected?			0
Carbon 14 age	:	Unknown	0
Wellhead Protection Score	:		55
Wellhead Protection Vulnerability Rat	ing:		VULNERABLE

Vulnerability Overridden





625 Robert St. N. St. Paul MN 55155 P.O. Box 64975 St. Paul MN 55164 - 0975

PWSID: 1190012 TIER: 1
SYSTEM NAME: Hastings WHP RANK:

WELL NAME: Well #6 UNIQUE WELL #: 00207643

COUNTY: Dakota	TOWNSH	IP NUMBER: 115 RANGE: 17 W	SECTION: 34 QUARTERS: CDDB
CRITERIA		DESCRIPTION	<u>POINTS</u>
Aquifer Name(s)	:	Jordan	
DNR Geologic Sensitivity Rating	:	High	0
L Score	:	0	
Geologic Data From	:	Well Record	
Year Constructed	:	1972	
Construction Method	:	Cable Tool/Bored	0
Casing Depth	:	240	5
Well Depth	:	332	
Casing grouted into borehole?		Unknown	0
Cement grout between casings?		Yes	0
All casings extend to land surface?		Yes	0
Gravel - packed casings?		No	0
Wood or masonry casing?		No	0
Holes or cracks in casing?		Unknown	0
Isolation distance violations?			0
Pumping Rate	:	1010	20
Pathogen Detected?			0
Surface Water Characteristics?			0
Maximum nitrate detected	:	11 05/06/1999	VULNERABLE
Maximum tritium detected	:	7.6 01/13/2004	VULNERABLE
Non-THMS VOCs detected?			0
Pesticides detected?			0
Carbon 14 age	:	Unknown	0
Wellhead Protection Score	:		25
Wellhead Protection Vulnerability Rat	ing :		VULNERABLE

Vulnerability Overridden :





625 Robert St. N. St. Paul MN 55155 P.O. Box 64975 St. Paul MN 55164 - 0975

PWSID: 1190012 TIER: 1
SYSTEM NAME: Hastings WHP RANK:

WELL NAME: Well #7 UNIQUE WELL #: 00509053

COUNTY: Dakota	TOWNSH	IP NUMBER:	RANGE:	SECTION:	QUARTERS:
CRITERIA		DESCRIPTION	<u>NC</u>		<u>POINTS</u>
Aquifer Name(s)	:	Jordan			
DNR Geologic Sensitivity Rating	•	High			0
L Score	:	0			
Geologic Data From	Ī	Data Inferred	d From Nearby Wells	3	
Year Constructed	:	1989			
Construction Method	:	Cable Tool/B	ored		0
Casing Depth	:	205			5
Well Depth	:	285			
Casing grouted into borehole?		Yes			0
Cement grout between casings?		Yes			0
All casings extend to land surface?		Yes			0
Gravel - packed casings?		No			0
Wood or masonry casing?		No			0
Holes or cracks in casing?		Unknown			0
Isolation distance violations?					0
Pumping Rate	:	1200			20
Pathogen Detected?					0
Surface Water Characteristics?					0
Maximum nitrate detected	:	6.3 02/08	3/2016		30
Maximum tritium detected	:	4.36 03/2	9/2016		VULNERABLE
Non-THMS VOCs detected?		Trichloroeth	ene (TCE)	03/03/1992	VULNERABLE
Pesticides detected?					0
Carbon 14 age	:	Unknown			0
Wellhead Protection Score	:				55
Wellhead Protection Vulnerability Rat	ing:				VULNERABLE
Vulnerability Overridden	:				Jim Walsh





625 Robert St. N. St. Paul MN 55155 P.O. Box 64975 St. Paul MN 55164 - 0975

PWSID: 1190012 TIER: 1
SYSTEM NAME: Hastings WHP RANK:

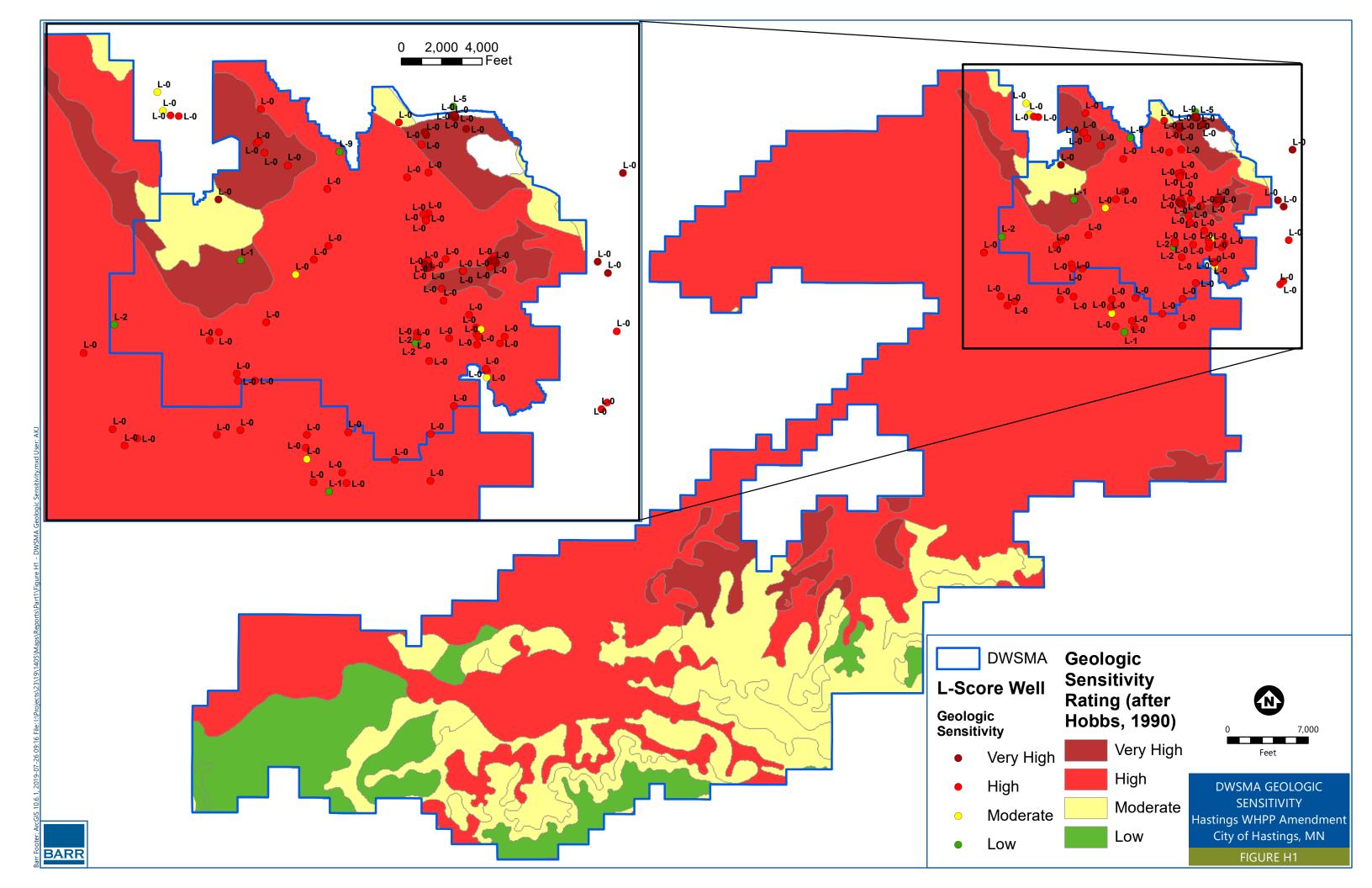
WELL NAME: Well #8 UNIQUE WELL #: 00686266

COUNTY: Dakota	TOWNSH	IP NUMBER:	RANGE:	SECTION:	QUARTERS:
CRITERIA		DESCRIPTION	<u>NC</u>		<u>POINTS</u>
Aquifer Name(s)	:	Jordan			
DNR Geologic Sensitivity Rating	:	High			VULNERABLE
L Score	:	0			
Geologic Data From	:	Well Record			
Year Constructed	:	2006			
Construction Method	:	Cable Tool/B	ored		0
Casing Depth	:	188			10
Well Depth	:	280			
Casing grouted into borehole?		No			0
Cement grout between casings?		Yes			0
All casings extend to land surface?		Yes			0
Gravel - packed casings?		No			0
Wood or masonry casing?		No			0
Holes or cracks in casing?		Unknown			0
Isolation distance violations?					0
Pumping Rate	:	1200			20
Pathogen Detected?					0
Surface Water Characteristics?					0
Maximum nitrate detected	:	9 10/02/2	013		30
Maximum tritium detected	:	Unknown			0
Non-THMS VOCs detected?					0
Pesticides detected?					0
Carbon 14 age	:	Unknown			0
Wellhead Protection Score	:				60
Wellhead Protection Vulnerability Rat	ing :				VULNERABLE

Vulnerability Overridden :

### Appendix H

**Aquifer Vulnerability Supporting Information** 



### Appendix I

**Groundwater Model Files and GIS Shapefiles**